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TECHNICAL NOTE

LOW-SPEED AERODYNAMIC CHARACTERISTICS OF A MODEL OF A
HYPERSONIC RESEARCH AIRPLANE AT ANGLES OF ATTACK

UP TO 90° FOR A RANGE OF REYNOLDS NUMBERS

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SUMMARY

Static force tests have been made at low subsonic speeds for a model of a hypersonic research airplane in the Langley high-speed 7-by 10-foot tunnel to determine the aerodynamic forces and moments up to an angle of attack of 90° for a range of Reynolds numbers. The Reynolds numbers, based on the mean aerodynamic chord, ranged from 740,000 to 1,900,000, which correspond to dynamic pressures from 15 to 100 lb/sq ft (Mach numbers from 0.10 to 0.27). The model was tested in the clean configuration with various horizontal-tail settings, horizontal tail off, lower rudder off, fuselage alone, and with various size strakes and slats on the nose of the model. Representative results of the present investigation are presented in plotted form, and a tabulation of all the data obtained is presented in a table. Appreciable effects on side force, yawing moment, and pitching moment are indicated by changes in Reynolds number for angles of attack of 40° to 90°.

INTRODUCTION

In recent years, there has been increasing interest in large-angle motions of airplanes at high attitude angles. The analyses of dynamic-model tests related to these motions are becoming very difficult without the aid of force-test data at high attitude angles. Also, such data are essential for analytical studies of large-angle motions. The present investigation was undertaken to measure the forces and moments on a model of a modern research airplane. The tests were made at subsonic speeds and were conducted in the Langley high-speed 7- by 10-foot tunnel for angles of attack from 0° to 90° and for sideslip angles from 10° to -30°. The Reynolds numbers covered in the investigation ranged from 740,000 to 1,900,000, based on the mean aerodynamic chord, or 335,000 to 865,000, based on the maximum depth of the fuselage, which correspond to dynamic pressures of 15 to 100 lb/sq ft (Mach numbers from 0.10 to 0.27). Since the majority of the data discussed is for

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high angles of attack and since the larger effects of Reynolds number are obtained at these angles of attack, the Reynolds numbers referred to are generally based on the maximum depth of the fuselage.

Spin and recovery characteristics of many airplane designs have been evaluated reliably based on tests of small dynamic models in the spin tunnel. However, due to configuration changes leading to long nose lengths on airplanes, special cognizance must be taken of possible significant effects of Reynolds number. The magnitude of the side force on the fuselage portion forward of the wing-fuselage intersection (hereinafter referred to as the nose) may have large variations with Reynolds number depending on the cross section of the nose with a resulting variation in yawing moment and a corresponding damping or propelling influence in the spin (refs. 1 to 3). Although the tests were made primarily to assist in the evaluation of the spin and recovery characteristics of the present configuration, the results are considered to be of general interest.

SYMBOLS

The aerodynamic coefficients of this investigation are referenced to the body system of axes shown in figure 1. The moment coefficients are given about a moment center corresponding to 20 percent of the wing mean aerodynamic chord.

$\mathtt{C}_{\mathbf{N}}$	normal-force coefficient, $\frac{-F_{\rm Z}}{q{\rm S}}$
${\tt C}_{\tt A}$	axial-force coefficient, $\frac{-F_X}{qS}$
$C_{\mathbf{m}}$	pitching-moment coefficient, $\frac{M_{\underline{Y}}}{qS\overline{c}}$
Cl	rolling-moment coefficient, $\frac{M_{X}}{qSb}$
$C_{\mathbf{n}}$	yawing-moment coefficient, $\frac{M_Z}{qSb}$
$C_{\mathbf{Y}}$	lateral-force coefficient, $\frac{F_{\mbox{\scriptsize Υ}}}{q\mbox{\scriptsize S}}$
$C_{\mathbf{Y}_{\beta}} = \frac{\partial C_{\mathbf{Y}}}{\partial B}$	

$$C_{n_{\beta}} = \frac{\partial C_{n}}{\partial \beta}$$

L/D

ratio of lift to drag

M_{X}	rolling moment acting about X body axis, ft-lb
M_{Υ}	pitching moment acting about Y body axis, ft-lb
M_{Z}	yawing moment acting about Z body axis, ft-lb
F_{X}	longitudinal force acting along X body axis, 1b
F_{Y}	lateral force acting along Y body axis, lb
F_{Z}	normal force acting along Z body axis, 1b
ъ	wing span, ft
ē	wing mean aerodynamic chord, ft
q	dynamic pressure, $\frac{\rho V^2}{2}$, lb/sq ft
	<u>_</u>
М	Mach number
M S	Mach number wing area, sq ft
. *	
S	wing area, sq ft
s v	wing area, sq ft free-stream velocity, ft/sec
S V	wing area, sq ft free-stream velocity, ft/sec air density, slugs/cu ft
S V P	wing area, sq ft free-stream velocity, ft/sec air density, slugs/cu ft maximum depth of fuselage at wing-fuselage intersection, ft
S V P l	<pre>wing area, sq ft free-stream velocity, ft/sec air density, slugs/cu ft maximum depth of fuselage at wing-fuselage intersection, ft kinematic viscosity, sq ft/sec</pre>
S V P l	wing area, sq ft free-stream velocity, ft/sec air density, slugs/cu ft maximum depth of fuselage at wing-fuselage intersection, ft kinematic viscosity, sq ft/sec angle of attack of fuselage center line, deg

R Reynolds number, $\frac{Vl}{v}$ or $\frac{V\overline{c}}{v}$

 $\delta_{\mbox{\scriptsize H}}$ deflection of horizontal tail, positive when trailing edge down, deg

MODEL DESCRIPTION

A drawing of the model is shown in figure 2 and the dimensional characteristics are given in table I. The model was tested in the clean configuration with various horizontal-tail settings, horizontal tail off, lower rudder off, fuselage alone, and with various size strakes and slats on the nose of the model. The strakes and slats were made of 1/16-inch-thick metal, and the location and size of the strakes and slats tested are shown in table II and figures 3 and 4.

TESTS, CORRECTIONS, AND ACCURACY

Tests

The model was mounted on a six-component internal strain-gage balance in the Langley high-speed 7- by 10-foot tunnel and was supported with a U-shape, sting support system. A sketch of the model support system is shown in figure 5, and photographs are shown in figure 6. As previously indicated, the tests were conducted for an angle-of-attack range of 00 to 900 and for a range of sideslip angles of 10° to -30° ; the Reynolds numbers, based on the maximum depth of the model fuselage nose section, ranged from 335,000 to 865,000 which correspond to a dynamic pressure of 15 to 100 lb/sq ft. For convenience, a plot of dynamic pressure against Reynolds number as presented in figure 7.

The desired combination of angle of attack α and sideslip β could not be obtained for a given run without going into the test section of the tunnel and changing the model roll angle \emptyset with each change in the turntable angle α_1 . Of course, the time required for this type of operation would be prohibitive; therefore, the model tests were made by setting the model at a given roll angle and rotating the turntable through its angle range by remote control. Constant values of angle of attack were then obtained for given values of sideslip by cross-plotting. The relationship of angle of attack and angle of sideslip with turntable angle and roll angle are shown in figure 8.

Corrections

Blockage corrections, as determined by reference 4, were applied to the dynamic pressure. The model angles of attack and sideslip have been corrected for deflection of the balance and sting support under load. The jet-boundary corrections were not applied to the angle of attack; the maximum angle of attack increase due to the jet-boundary-correction method of reference 5 would be about 0.35°. This increase occurs at an angle of attack of about 40° and decreases to zero as a approaches 90° .

Accuracy

The accuracy of the measurement of the forces and moments has been computed based on the maximum load limits of the strain-gage balance used, and is as follows:

C_{NI}																						_								±0.0300
																														-
^{C}A	•	•	•	•	•	•	•	٠	•	•	•	•	•	•	•	•	•	•	•	•	•	•	٠	•	•	•	•	•	•	±0.0021
$^{ m C}_{ m m}$	•	٠	•	•	•	•	•	•			•	•			•			•												±0.0040
$^{\mathtt{C}}$	•	•	٠	•	•	•	•		•	•	•	•	•	•	•	•		•												±0.0009
$\mathtt{c}_\mathtt{n}$	•		•			•						٧																		±0.0009
																														±0.0063

RESULTS AND DISCUSSION

Representative results of the present investigation are presented in figures 9 to 16, and a tabulation of all the data obtained and an explanation of the code for the various configurations tested are presented in table III. The data were reproduced from an automatic computing machine, and the minus signs are to the right of the numbers to which they apply.

The longitudinal coefficients are presented in figures 9 and 10 and indicate that an appreciable effect of Reynolds number is obtained for the pitching moment. The major effect of Reynolds number on pitching moment is shown to be in the angle-of-attack range from 30° to 75° and indicates larger nose-down pitching moments for higher Reynolds numbers. The relatively small effects of Reynolds number on the normal force are considered to be in the right direction from the effects seen on pitching moment. The apparent effects of Reynolds number on axial force between angles of attack of 40° and 90° are relatively large percentagewise, but the actual value of the coefficient for either the low or high Reynolds numbers would probably be insignificant at these attitudes.

The lateral coefficients are presented on figures 11 to 13. Figure 11 shows little or no effect of Reynolds number on the rollingmoment coefficient C_l , whereas figures 12 and 13 indicate that relatively large effects of Reynolds number may be expected on the side-force coefficient C_Y and yawing-moment coefficient C_n . Figure 12 shows that, for the angle-of-attack range between 40° and 70°, smaller negative values of C_{Y_β} were obtained for the higher Reynolds numbers. Test results indicate that the largest effect of Reynolds number on yawing moment is between angles of attack of 50° and 70° (fig. 13). In general, C_{n_β} was more positive (or less negative) for the higher Reynolds numbers.

The data of figures 11 to 13 indicate that large variations in side-force, yawing-moment, and rolling-moment coefficients are possible at a sideslip angle of 0° for low Reynolds numbers and relatively high angles of attack. For example, the side-force coefficient at a Reynolds number of 335,000 and an angle of attack of 60° may vary from 0.15 to -0.24. These results might be explained by asymmetrical vortices being shed from the nose as suggested in reference 6. It should be emphasized, therefore, that in this range of Reynolds number and angle of attack, large asymmetric side forces and yawing moments are likely to occur at a sideslip angle of 0° for a given configuration, even to the extent of being of opposite sign.

As was previously indicated, the primary effect of Reynolds number on side force and yawing moment occurred at angles of attack from about 50° to 70° . In analyzing the results, it is to be expected that the wing and tail surfaces, at these high angles of attack, would be more like flat plates insofar as effects of Reynolds number are concerned, and in addition, these flat surfaces would be expected to spoil any effect of Reynolds number on the fuselage rearward of the wing leading edge. The nose section has no such surfaces to spoil the flow and is, therefore, more susceptible to various flow changes due to Reynolds number. As pointed out in references 2 and 3, large changes in side force due to Reynolds number can be obtained for various cross-sectional shapes for two-dimensional bodies. Somewhat similar effects of Reynolds number would be expected to occur on three-dimensional bodies such as the nose section. If the nose is then considered to cause most of the effects of Reynolds number, a positive yawing-moment increment would be expected. The increment in side force due to Reynolds number for an angle of attack of 60° (fig. 12) and an angle of sideslip of 7° is about 0.32. As can be seen from figure 13 (o = 60° ; β = 7°), a positive yawing-moment increment of about 0.18 is obtained. The lever arm of the side force, required to obtain this increment in yawing moment, is about three-fourths the nose length. It is considered, therefore,

that most of the effects of Reynolds number observed in side force and yawing moment were caused by the nose section.

In order to determine if the range of Reynolds numbers had been sufficiently covered, side-force coefficients were plotted against Reynolds number for the spinning angle-of-attack range of the model (400 to 90°) in figure 1 4 . Side force was chosen because of its large variation with increasing Reynolds number for cylinders of various cross-sectional shapes. (See refs. 2 and 3.) The test results indicate that for a sideslip angle of 0 the critical Reynolds number region, based on the maximum fuselage depth, was between 500,000 and 600,000.

However, for sideslip angles of 50 to -200, figure 14 indicates that the critical Reynolds number region increases. This effect agrees with three-dimensional static data of other designs (unpublished) at high angles of attack which show an increase in the critical Reynolds number region with increase in sideslip angle. At the lower Reynolds numbers, the side-force slope indicates that the subcritical region was not obtained completely. It should be pointed out that even though the results of this investigation indicate a given effect of Reynolds number for this design, other designs which have different fuselage cross-sectional shapes would be expected to have different critical Reynolds number regions.

In an effort to obtain an indication of the type and size of an auxiliary control device which would be required to make the side force and yawing moment acting on the spin-tunnel model (R = 50,000) more nearly representative of the side force and yawing moment present on the full-scale airplane (R $\approx 8 \times 10^6$), strakes and slats were placed on the nose of the force test model and tested at a Reynolds number of about 335,000. Strakes were used as transition strips to change the air flow, and slats were used to direct the air flow (figs. 3 and 4). A representative plot showing the effects of a strake (B-2R) on side force, at an angle of attack of 70°, is shown on figure 15. As can be seen from this figure, a side-force increment of about -0.35 is indicated between the minimum and maximum Reynolds numbers of the present investigation. The increment added by the B-2R strake is approximately -0.30 and allows the data for the low Reynolds numbers to represent more closely the characteristics of the high Reynolds numbers. Indications are, therefore, that a strake approximating the size and location of the B-2R strake could be used on the dynamic spin model to aid in correcting effects of Reynolds number on side force and yawing moment at spinning angles of attack (40° to 90°) and a range of sideslip angles of ±150.

Brief tests were made to determine the effects of the lower rudder on the value of maximum trim $\ L/D$ and the angle of attack at which it

takes place. These results are presented on figure 16. These tests were made at a dynamic pressure of 100 lb/sq ft (R = 1,900,000 based on \bar{c}) with the model in the clean condition, landing gear retracted. Test results indicate that the maximum (L/D trim was somewhat greater with the lower rudder off than with it on but both occurred at an angle of attack of about 6° .

CONCLUDING REMARKS

Based on a static force test investigation for a range of Reynolds numbers on a model of a modern research airplane configuration, the following is concluded:

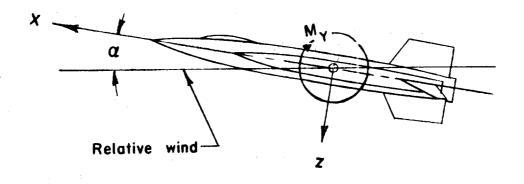
- l. For an angle-of-attack range of 40° to 90° and sideslip angle of 0° , the critical Reynolds number region, based on the maximum depth of the fuselage, for side-force coefficient C_Y and yawing-moment coefficient C_n is between 500,000 and 600,000.
- 2. In general, for sideslip angles of 5° to -20°, the critical Reynolds number, based on the maximum fuselage depth, is greater than 800,000.
- 3. Large increments in pitching moment are obtained due to change in Reynolds number for the angle-of-attack range from 30° to about 75°. Higher Reynolds numbers indicate larger nose-down pitching moments.
- 4. Effects of Reynolds number on normal and axial forces and on rolling moment were found to be small.
- 5. Large increments in yawing moments and side force were obtained for the range of Reynolds numbers tested for angles of attack of 50° to 70° .
- 6. For an angle-of-attack range of 40° to 60° , and at low Reynolds numbers, large asymmetric side forces and yawing moments are likely to occur at a sideslip angle of 0° for a given configuration, even to the extent of being of opposite sign.
- 7. It was found that a strake placed on the nose of the model helped to compensate for the effects of Reynolds number on side force and yawing moment.

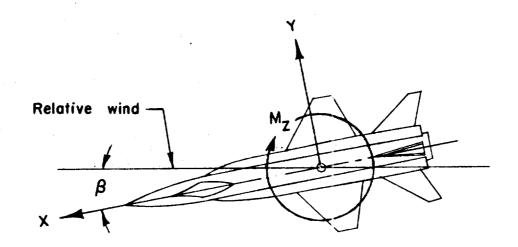
Langley Research Center,
National Aeronautics and Space Administration,
Langley Field, Va., March 24, 1960.

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- 3. Polhamus, Edward C., Geller, Edward W., and Grunwald, Kalman J.:
 Pressure and Force Characteristics of Noncircular Cylinders as
 Affected by Reynolds Number With a Method Included for Determining
 the Potential Flow About Arbitrary Shapes. NASA TR R-46, 1959.
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- 6. Letko, William: A Low-Speed Experimental Study of the Directional Characteristics of a Sharp-Nosed Fuselage Through a Large Angle-of-Attack Range at Zero Angle of Sideslip. NACA TN 2911, 1953.





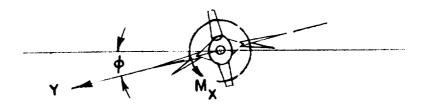


Figure 1.- Body system of axes and related angles.

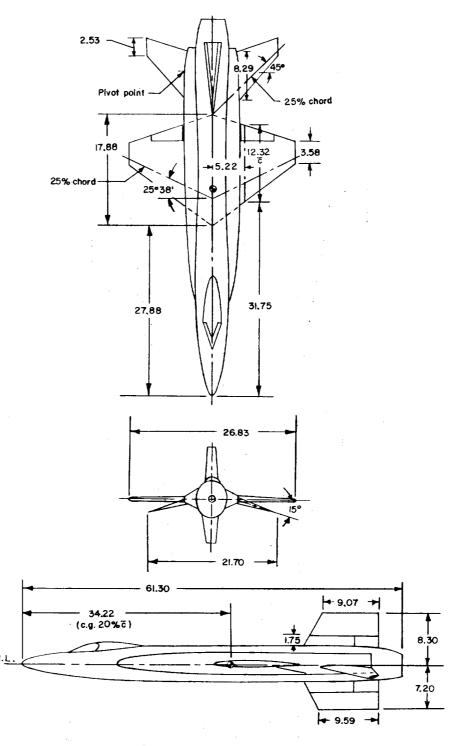


Figure 2.- Three-view drawing of the model. (All dimensions are in inches.)

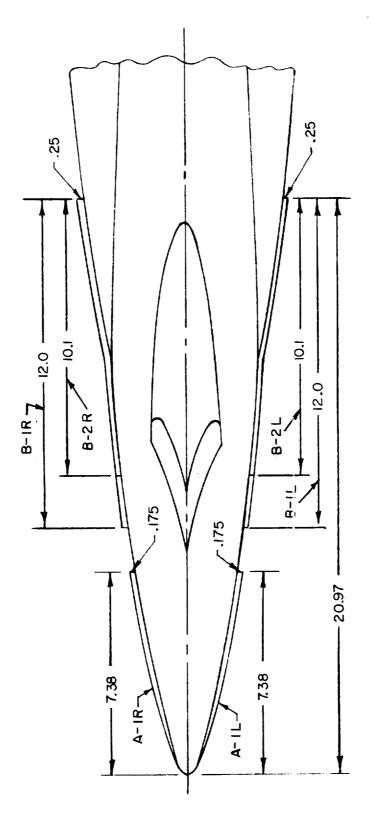


Figure 3.- Sketch of nose of model indicating size and location of strakes. (Strakes located on fuselage reference line; all dimensions are in inches.)

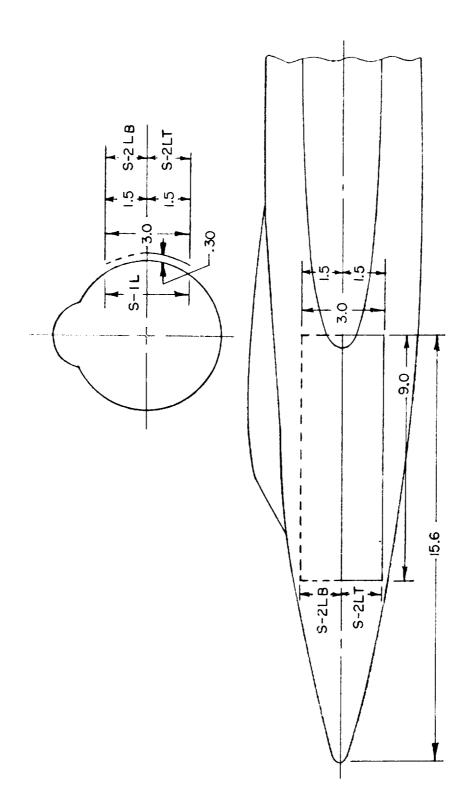


Figure 4.- Two-view sketch of nose indicating size and location of slats. (All dimensions are in inches.)

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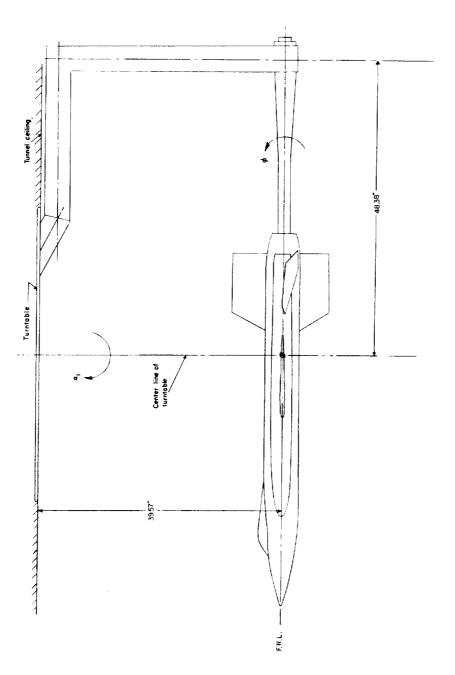
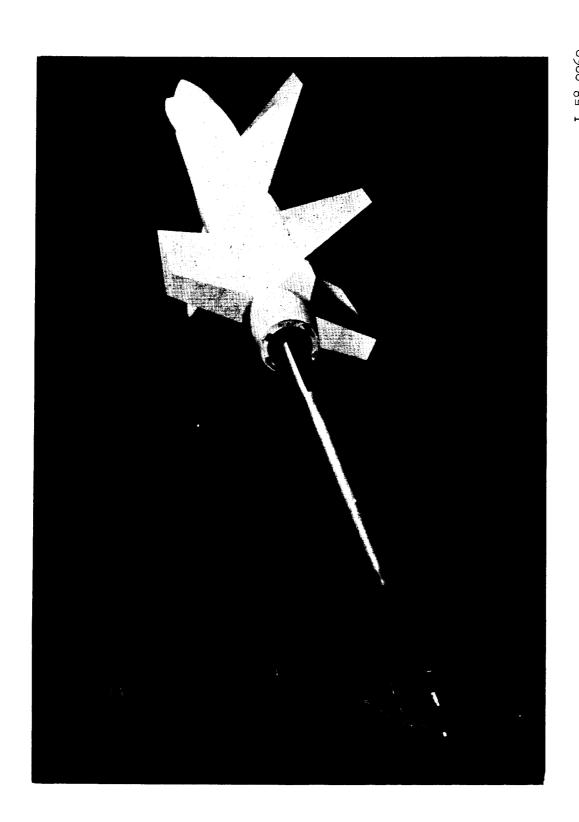


Figure 5.- Sketch showing model and sting arrangement used in Langley high-speed 7- by 10-foot tunnel.

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I-58-2269 Figure 6.- Photographs of research model mounted on sting in Langley high-speed 7- by 10-foot tunnel.

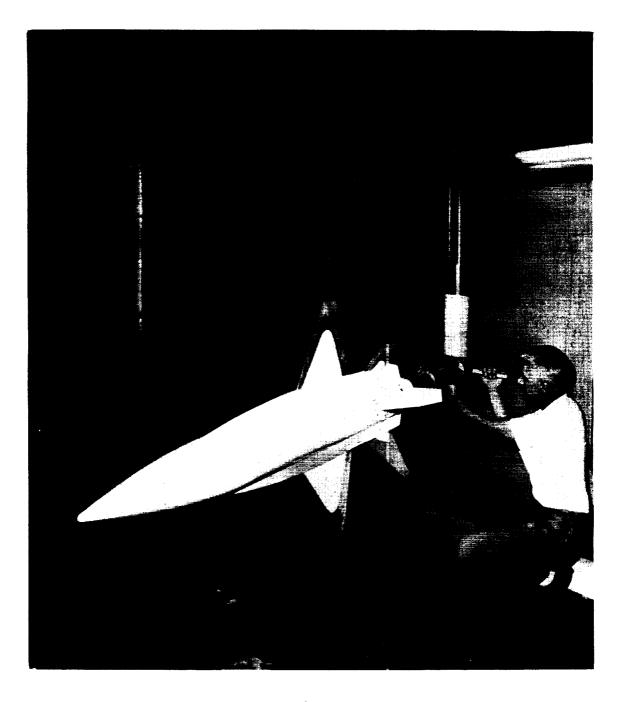


Figure 6.- Concluded.

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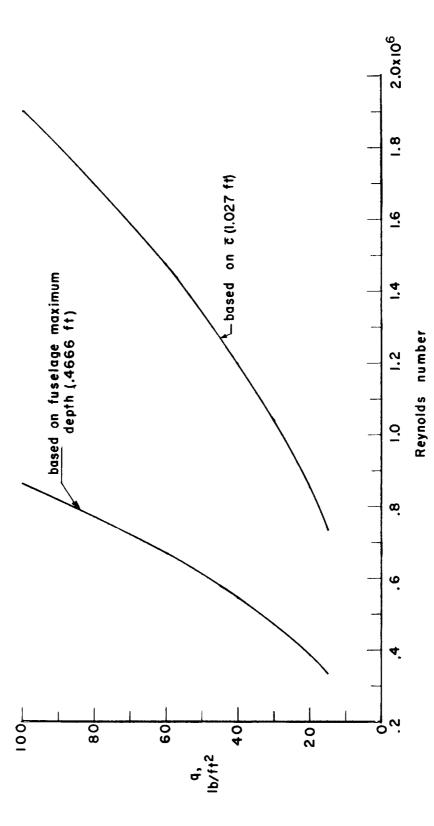


Figure 7.- Variations of Reynolds number with dynamic pressure.

 $\beta = \sin^{-1} (\sin \alpha_1 \sin \phi)$ $\alpha = \tan^{-1} (\tan \alpha_1 \cos \phi)$

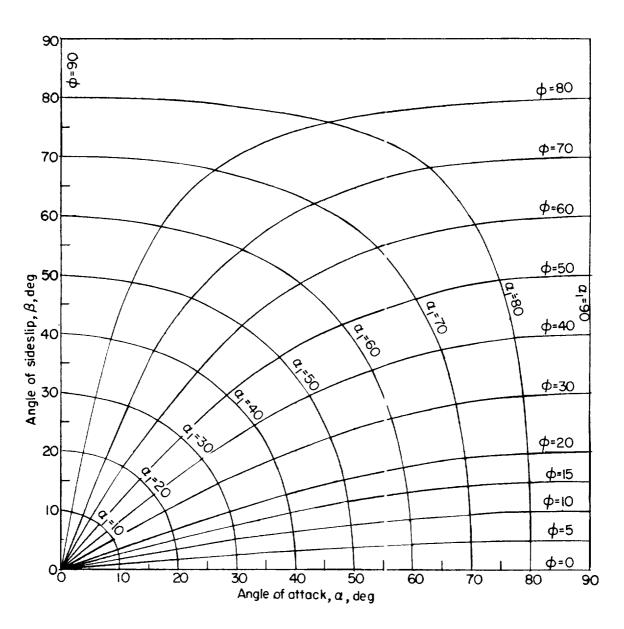
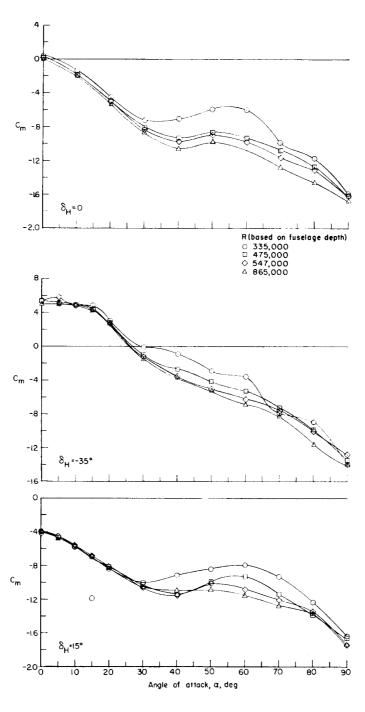


Figure 8.- Plot showing relationship of turntable angle and roll angle to angle of attack and sideslip.

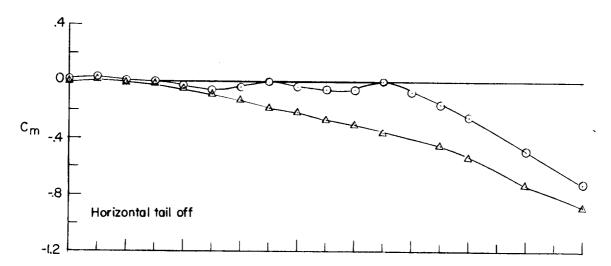


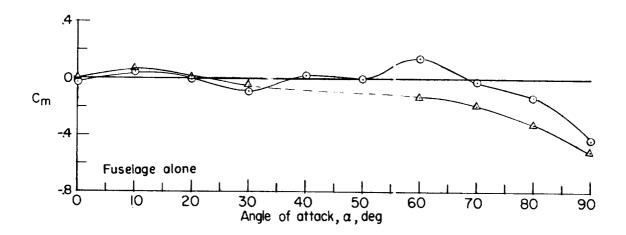
(a) Complete model.

Figure 9.- Variations of pitching-moment coefficient with angle of attack and Reynolds number for various horizontal-tail positions. (β = 0; center-of-gravity location, 20 percent \bar{c} .)

R(based on fuselage depth)

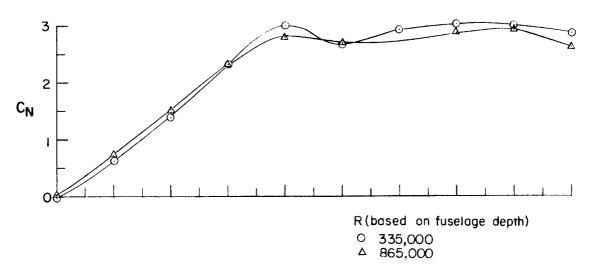
○ 335,000 △ 865,000





(b) Horizontal tail off and fuselige alone.

Figure 9.- Concluded.



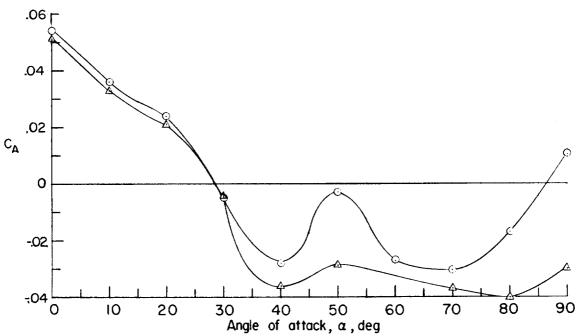


Figure 10.- Representative variations of the normal- and axial-force coefficients with angle of attack for the minimum and maximum Reynolds numbers tested. (Complete model, $\beta=0$.)

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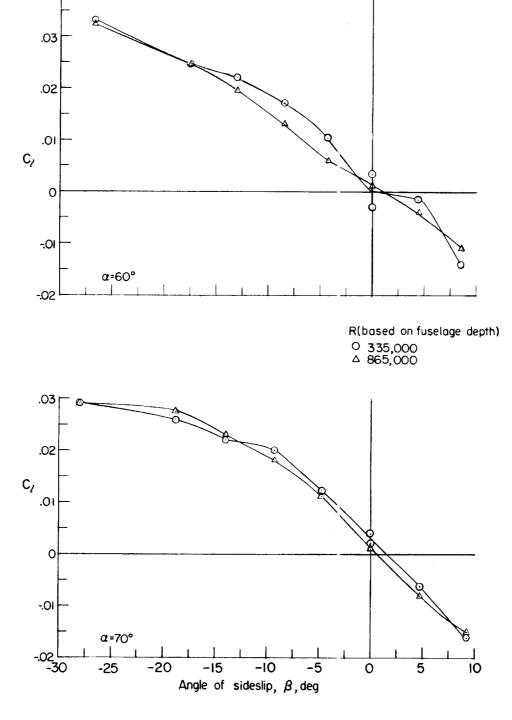


Figure 11.- Variation of rolling-moment coefficient with sideslip for the maximum and minimum Reynolds numbers tested. (Complete model.)

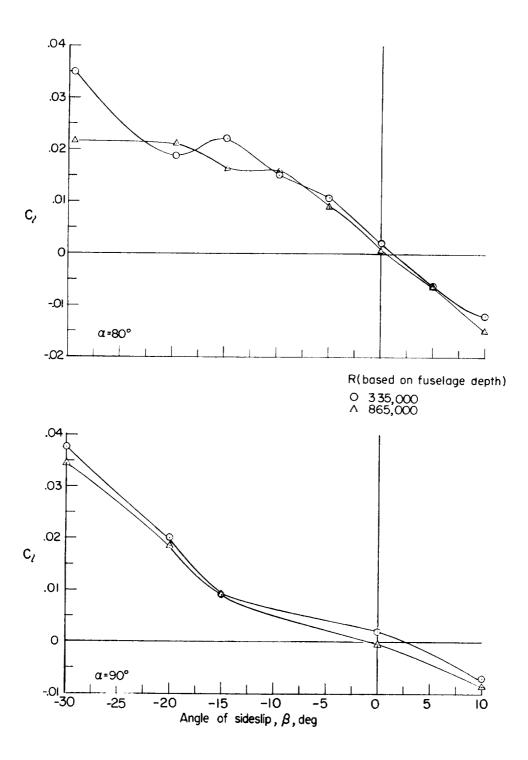


Figure 11.- Concluded.

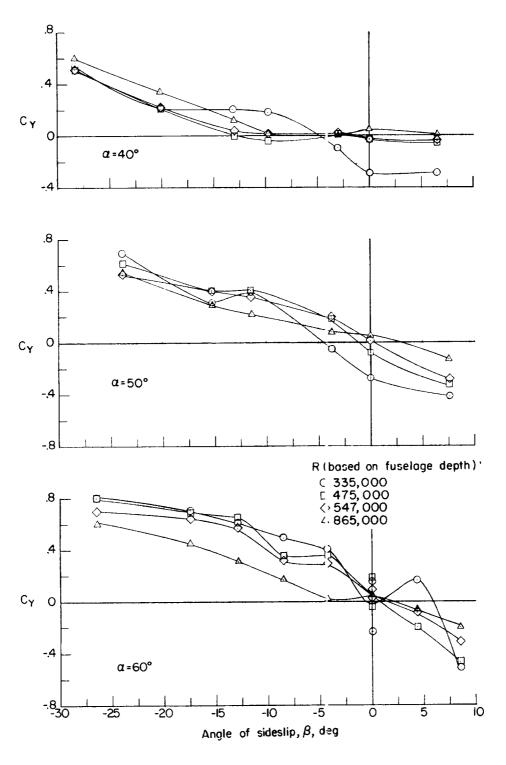


Figure 12.- Variation of side-force coefficient with sideslip for various Reynolds numbers and angles of attack. (Complete model.)



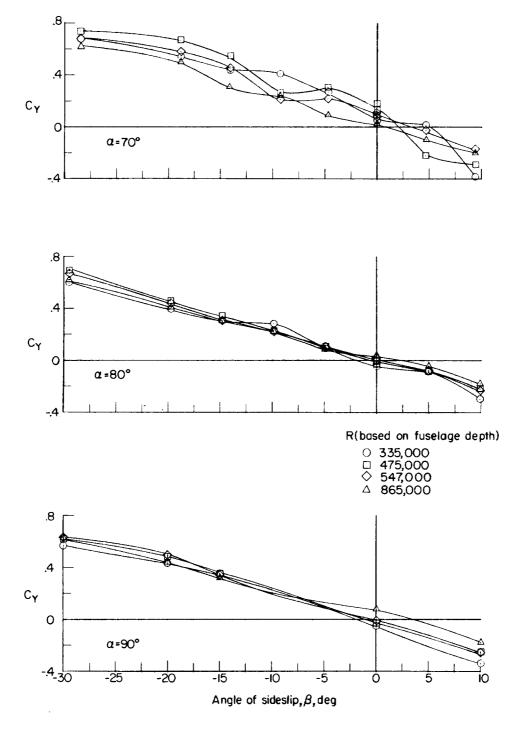


Figure 12.- Concluded.

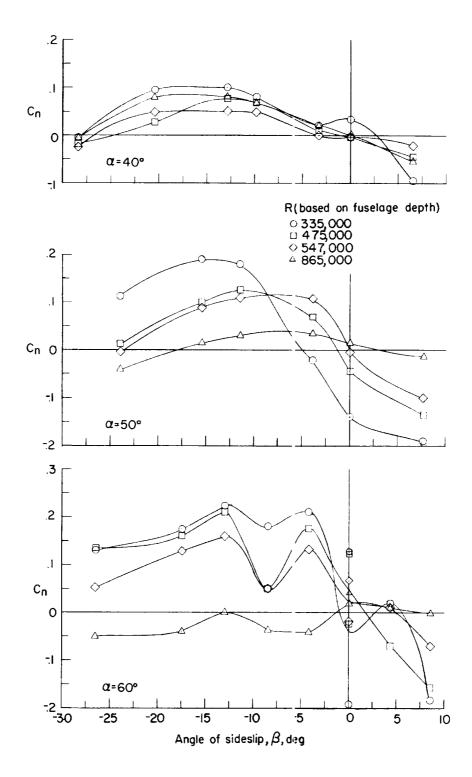


Figure 13.- Variation of yawing-moment coefficient with sideslip for various Reynolds numbers and angles of attack. (Complete model.)

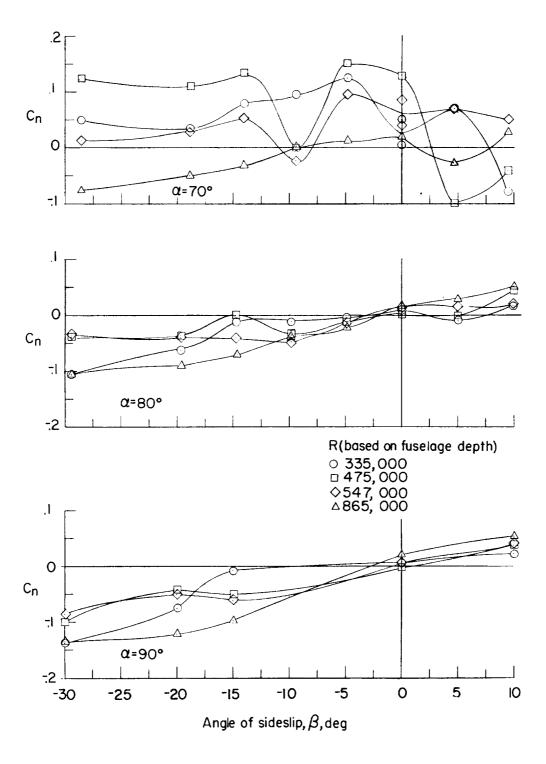


Figure 13.- Concluded.

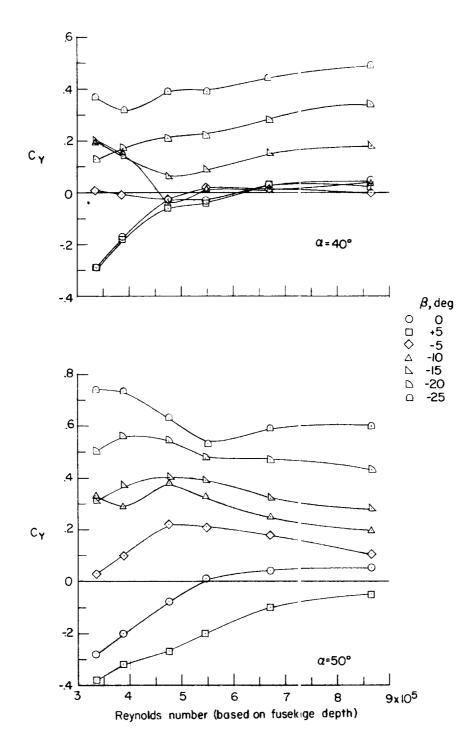
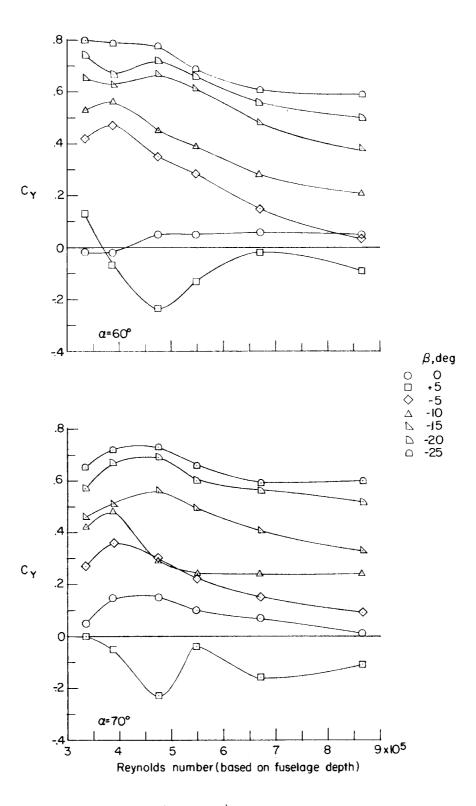


Figure 14.- Variation of side-force coefficient with Reynolds number for various sideslip angles and angles of attack. (Complete model.)



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Figure 14.- Continued.

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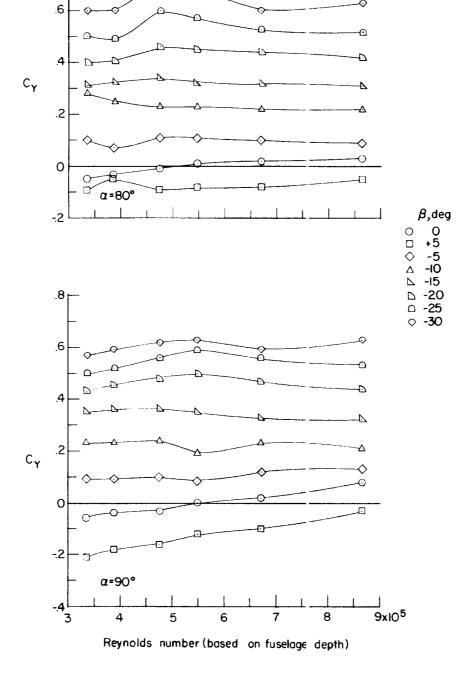


Figure 14.- Concluded.

	R(based on fuselage	depth)
0	Clean model	335,000
	Clean model	865,000
\Diamond	With strake B-2R	335,000

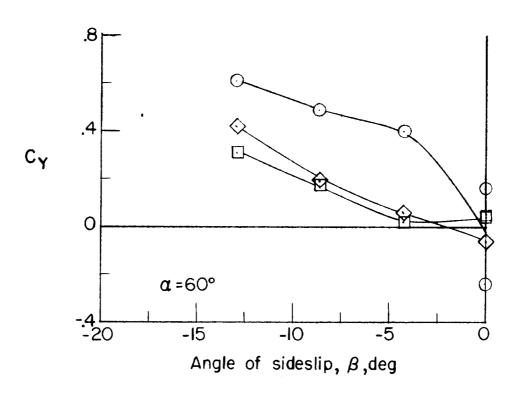


Figure 15.- Representative variation of side-force coefficient with sideslip angle showing strake effectiveness.



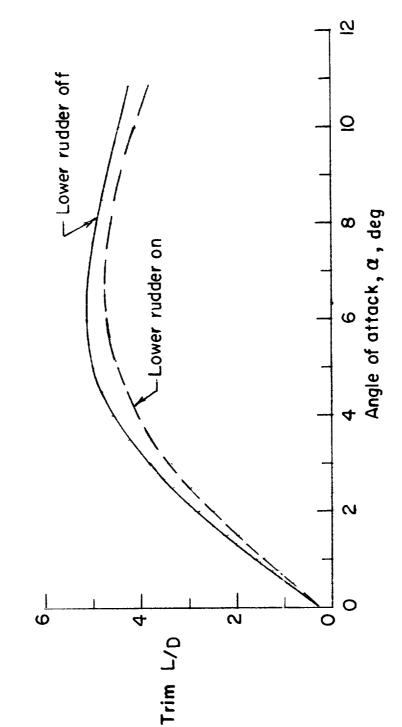


Figure 16.- Variation of trim lift-drag ratio with angle of attack.

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TABLE I.- DIMENSIONAL CHARACTERISTICS OF MODEL

Overall length, ft	5.13
Wing:	
Area, sq ft	2.00
Span, ft	2.24
Aspect ratio	2.50
Mean aerodynamic chord, in	
Sweepback (25-percent-chord line), deg	
Incidence, deg	C
Dihedral, deg	C
Horizontal tail:	
Area (exposed), sq ft	0.52
Span, ft	
Sweepback (25-percent-chord line), deg	
Dihedral, deg	
Vertical tail (upper):	0 1.2
Area (exposed), sq ft	0.41
Sweepback (leading edge), deg	
Movable tail area, sq ft	0.26
Vertical tail (lower):	
Area (exposed), sq ft	0.34
Movable tail area, sq ft	0.20
Sweepback (leading edge), deg	30.00
Maximum fuselage depth, ft	0.467

TABLE II.- SIZE AND LOCATION OF STRAKES AND SLATS

(a) Nose strakes (located on fuselage reference line)

Strake	Location on fuselage	Distance from nose to forward end of strake, in.	Distance from nose to rearward end of strake, in.	Approximate length, in.	Approximate width, in.
A-1L	Left side	0	7.38	7.38	0.175
A-lR	Right side	0	7.38	7.38	0.175
B-1L	Left side	8.97	20.97	12.00	0.250
B-1R	Right side	8.97	20.97	12.00	0.250
B-2L	Left side	10.87	20.97	10.10	0.250
B-2R	Right side	10.87	20.97	10.10	0.250

(b) Nose slats

[Distance from nose to forward end of slat, 6.6 in.; distance from nose to rearward end of slat, 15.6 in.; approximate length, 9.0 in.; approximate distance between fuselage curvature and slat, 0.30 in.]

Slat	Location on fuselage	Approximate width, in.	Distance from top of slat to fuselage reference line, in.
S-1L	Left side	3.0	1.5
S-1R	Right side	3.0	1.5
S-2LT	Left side	1.5	0
S-2RT	Right side	1.5	0
S-2LB	Left side	1.5	1.5
S-2RB	Right side	1.5	1.5

TABLE III. - AERODYNAMIC COEFFICIENTS OF MODEL FOR THE COMPLETE INVESTIGATION

Configuration Code

F':	irst	dí,	gi.	t:																												
	$Com_{\mathbf{F}}$	le	te	mo	ode	el																										-
	Fuse	la	ge	a.	loi	ne																										2
	Hori																															7
	Lowe																															ĺ
Se	econd	l d:	ig	it	(A i	an	d!	В	coi	ns	id	er	eđ	to	o 1	оe	pa	ar	t (of	se	ecc	ond	l d	lie	gi	t):	*			
	No s	tra	ake	e s	01	r	sl	at	S																							(
	A-lI]
	B-1I	٠ د																														2
	B-1R																															7
	B-2I																															Į.
	B-2R																															=
	S-1I																															6
	S-1R																															7
	S-2I																															8.A
	S-2R																															_
	S-2I																															
	S-2R																															9E
m					Ī	•	·	·	·	·	-	·	Ĭ	•	•		•	•	·	•	•		•	Ī	•	•	•	•	•	•	•	71
Tr	ird																															_
	$\delta_{\mathrm{H}} =$	0	,	•	•	•	•	•	•	•	•	•	•	•	•	•	•	٠	•	•	•	•	٠	•	•	•	•	•	•	•	•	С
	δ _H =	_1	0				•							•		•											•	•	•	•		2
	δ _H =	- 8	30										•			•																4
	δ _H =																															6
	δ _H =	+]	-5°)				•										•														7

For example, configuration 18B4 means:

1 Complete model 8B S-2LB O $\delta_{\mathrm{H}} = 0^{\circ}$

 $^{^{\}star}$ See table II for explanation of code for strakes and slats.

TABLE III. - AERODYNAMIC COEFFICIENTS OF MODEL FOR THE COMPLETE INVESTIGATION - Continued

Config.	Run	Point	α ₁ , deg	ø, deg	q, lb/sq ft	ar, deg	β, deg	c _N	(A	C _m	C ₁	Cn	CY
160	ı	1	.60	.60	15.00	.00	۰υ۵	.0606-	.0.36	.0410	•0011	-6068	.0061-
100	1	2	.00	.00	20.00	.00	•00	.0574-	.0334	.0389	1100	6600 و	-0058-
100	1	3	.00	.00	40.00	.00	•00	.0123-	.0312	•0163	•0010	•0027	•0019~
100	1	4	•00	•0u	60.00	.00	•00	.0024-	•U508	•0111.	.0009	+0013	.0014-
100 100	1	5 42	.00	.00	30.00	.00	.00	.0083 .0174	.0512 .0506	.0057 .0018	.0007	•0009 •0101	.0340-
100	2	6	10.00		15.00	10.03	.00	.6306	.0360	+1345-	.0016	-0017	.0039
100	2 2	7 8	10.00	.00	40.00	10.04	.00	.6719 .6919	•0357 •0333	•1525- •1677-	.0009	•0008 •0003	.0063 .0072
100	2	9	10.00		60.00	10.15	.00	7153	.6325	-1804-	.0008	.0007	.0018
100	2	10	10,00	•60	100.00	10.26	.00	.7322	.6327	.1882-	.0009	.0000	.0017
100	2	41	10.00	-60	30.00	10.07	•00	.7053	.0339	-1768-	.0007	•0079	•0242-
100	3	11	20.00	•00	15.00	20.08	.00	1.3895	.c238	.4532-	•0010	-0009	-0050
100	3	12	20.00	•00	20.00	20.10	•00	1.3989	.0257	.4915~ .4995~	.0006	-8000	.0106 .0015-
100	3	13 14	20.00 20.00	.00	60.00	20.21	•00	1.4140	.0225 .0220	-5126-	.0007 .0008	.0025 .0011	.0005-
165	3	15	20.00		100.00	20.56	.00	1.5231	.0214	.5330-	.0005	.0002-	.0005
100	3	40	20.00	.00	30.00	20.16	•00	1.4269	.0116-	-5064-	.0002-	•0092	.0268-
100	4	16	30.00	•60	15-16	30.13	.00	2.3285	.0056-	.7217-	.0013	-0004-	.0002
100		17	30.00	•00	20.21	30.17	•00	2.2298	.0012-	• 7666-	.0005	•0077	•0153
100	:	18 19	30.00 30.00	.00	40.42 60.64	30.33	.00	2.1873	.0023-	.8297- .8493-	.0006-	•0077- •0002	.0058-
100	:	20	30.00		101.06	30.87	.00	2.3128	.0046-	.8619-	0015	-0069-	0287
100	4	39	30.00	.00	30.32	30.25	•00	2.2009	.0000	.8119-	.0018-	+0041	.0137-
100	5	21	40.00	•00	15.34	40.17	•00	3.0153	.0283-	.7051-	-0355-	.0319	-2980-
100	5	22	40.00	.00	20.45	40.22	•00	2.8667	-0351-	.7661-	•0146-	•0023-	•1731-
100	5	23 24	40.00	•00	40.90 61.35	40.41	•00	2.6921 2.7598	.0107- .0139-	1.0549-	.0098	.0045- .0095	.0185~ .0242
100	5	25	40.00		102.25	41.07	•00	2.8251	C 157-	1.0549-	.0075-	.0009	-0567
100	5	38	40.00	.40	30.68	40.31	•00	2.7469	.0123-	•9305-	.0084	.0006	.0294-
100	6	26	50.00	0	15.57	50.15	•90	2.6664	-0)27-	•5950-	.0109-	•1426-	.2737-
100	6	27	50.00		20.76	50.21	•00	2.6963	-0151-	•5926-	.0072	•0983-	-1935-
100	6	28 29	50.00	.00	41.53 62.29	50.41 50.61	•00	2.6702	•0262- •0273-	.8958- .9508-	.0008 .0019	+0046- +0251	.0168
100	اة	30	50.00	.00	103.82	51.04	•00	2.7070	6287-	.9816-	.0020	.0149	.0479
100	6	37	50.00	•00	31.15	50.32	•00	2.7399	-0130-	.8634-	-0112	·C349-	.0733-
100	7	31	60.00	.00	15.83	60.17	•00	2.9237	.0271-	.6021-	-0036-	•1930-	-2409-
100	7 7	32 33	60.00 60.00	.00	21.10 42.20	60.22	•00	2.8646	•0364- •0386-	•7411- •9854-	.0019-	•1468- •0227-	.2218- .0169-
100	7	34	60.00	.00	63.30	60.66	•00	2.8030	.0,44-	1.0658-	.0024	.0345	.0594
100	7	36	60.00	.00	31.65	60.33	•00	2.7738	.0149-	•9312-	.0015	•0290-	•0490-
100	8	خ 4	70.00	.00	16.13	70.18	•00	3.0646	-0306-	•9791-	.0047	•0997	-0510
100	8	44	70.00	.00	21.50	70.23	•00	2.9218	•0336-	•9896-	-0045	•1346	•1314
100	8 8	45 46	70.00 70.00	.00	32.25 43.00	70.34 70.45	•00	2.8308 2.8319	.0109- .0107-	1.0860- 1.1646-	.0052 .0039	•1282 •0844	.1358 .0863
100	8	47	70.00	0	64.50	70.69	•00	2.8827	0136-	1.2436-	.0021	.0433	.0462
100	8	48	70.00	.65	107.50	71.14	•00	2.8697	.0372-	1.2748-	.0011	•0162	.0297
106	9	49	80.00	.00	16.22	80.19	•00	3.0305	.0172-	1.1701-	-0022	•0066	-0528-
100	9	50	80.00	•00	21.62	80.24	•00	3.0031	.0249- .0233-	1.1822-	•0026	•0028-	•0447- •0262-
100	9	51 52	80.00 80.00	•00	32.43 43.24	80.36 80.46	•00 •00	2.8820 2.8558	•0:33- •0:40-	1.2750-	.0025 .0028	.0032~ .0114	.0262
100	9	53	80.00	.00	64.86	80.70	•00	2.8791	0130-	1.3708-	.0019	.0069	.0117
100	9	54	80.00	.00	108.10	81.18	•00	2.9118	.0.04-	1.4582-	.0013	•0185	•0389
100	10	55	90.00	•00	16.28	90.17	•00	2.8692	-0104	1.5946-	.0015	-0064	.0518-
100	10	56	90.00	.00	21.70	90.23	•00	2.8612	.0371	1.5922~	.0018	.0033	-0430-
100	10 10	57 58	90.00	.00	32.55 43.40	90.33	•00	2.7745 2.7418	.0121- .0103-	1.6209-	.0009 .0012	•0004- •0068	*0062-
100	10	59	90.00	.00	65.10		•00	2.7261	-0:42-	1.6920-	2002	.0137	.0076
100	10	60	90.00	.00	108.50		•00	2.6405	.0100-			.0125	•0790
100	11	61	10.00	10.00	15.00	9.87	1.73	6079	.0355 .0348	•1279- •1522-	.0009-	•0143 •0145	.0421 -0427
100	11	62 63	10.00	10.60 10.60	20.00 30.00	9.89	1.74	•6447 •6486	.0348	1501-		·0145	.0427
100	11	64	10.00	10.00	40.00	9.94	1.75	6605	0123	-1584-	-0016-	-0143	0424-
100	11	65 66	10.00	10.00	60.00	9.99	1.75	.6885 .7159	.0318 .0313	•1717- •1827-	.0014-	.0151 .0138	.0472-
l			- '								1		
100	12	67	20.00 20.00	10.00	15.00 20.00	19.82	3.41 3.42	1.2767	.0:41 .0:63	.4028- .4545-	.0012-	.0000 .0002	.0678-
100	12	69	20.00	10.60	30.00	19.87	3.43	1.3432	.0:39	.4732-	.0010	-0031-	.0585-
100	12	70	26.00	10.00	40.00		3.44	1.3603	•0232	.4784-	.0009	+0048-	-0583
100	12	71 72	20.00	10.00	100.00		3.45 3.49	1.4084	0214	.4928- .5111-		.0067-	.0591-
100	**	''	20.00	10.00	100.00	-0.24	2.47	4.704	.0.00	• > 1.1.1-			. 0005
	L							1			l		

 $^{^{\}dagger}$ Minus signs are to the right of the numbers to which they apply.

TABLE III. - AERODYNAMIC COEFFICIENTS OF MODEL FOR THE COMPLETE INVESTIGATION - Continued

Config.	Run	Point	a_1 , deg	ø, deg	q, lb/sq ft	α, deg	β, deg	C _N	C _A	C _m	c,	Cn	C Y
100	13	73	30.00	10.60	15.16	29.74	5.00	2.2130	.0004-	•6875-	.0043	•0292-	•U198-
100	13	74 75	30.00 30.00	10.60	20.21 30.32	29.78	5.00	2.2001	.0007	-7368-	-0018-	.0287-	•0207-
100	13	76	30.00	10.60	40.42	29.86 29.93	5.01	2.1121	.0028	.8006- .8124-	.0025- .0071-	.0229- .0157-	.0180-
100	13	77	30.00	10.00	60.64		5.05	2.1925	.0009-	.8408-	.0028-	-0215-	6383
100	13	78	30.00	10.00	101.06	30.43	5.10	2.2147	.0033-	.8284	.0041-	•0237-	•0385- •0894-
100 100	14	79 80	40.00	10.00 10.00	15.34 20.45	39.71 39.76	6.43	2.7285	•0187- •0252-	•6844- •7605-	-0489-	•0867- •0487-	.2779- .1650-
100	14	81	40.00	10.00	30.68	39.86	6.45	2.7022	.0274-	.8917-	.0267-	.0444-	-0587-
100	14	82	40.00	10.00	40.90	39.94	6.46	2.5646	.0274-	.9860-			.0461-
100	14	83	40.00	10.00	61.35	40.16	6.49	2.6620	.0201-	1.0170-			.0276
100	14	84	40.00	10.60	102.25	40.58	6+54	2.7406	.0127-	1.0230-	.0075-	-0567-	.0070
100 100	15 15	85 86	50.00	10.00	15.57	49.72 49.78	7•66 7•66	2.6956	.0215-	•5099- •6503-	•0170-		-4128-
100	15	87	50.00	10.60	20.76	49.86	7.67	2.7414	.0226- .0141-	.6503- .8532-	•0169- •0061	•1848- •1336-	•3873- •3226-
100	15	88	50.00	10.60	41.53	49.95	7.68	2.5268	.0169-	•8797-	-0054	1002-	.2735-
100	15	89	50.00	10.00	62.29	50.15	7.71	2.5736	.0178-	.9332-	•0¢31	.0274-	1569-
100	15	90	50.00	10.00	103.82	50.56	7•75	2.6161	.0208-	•9624-	.0013-	-0048-	•1261-
100 100	16	91	60.00	10.60	15.83	59.77	8.66	2.6321	.0155-	•7300-	-0136	-1871-	•5107-
100	16 16	92 93	60.00	10.00 10.00	21.10 31.65	59.83 59.93	8 • 6 6 8 • 6 7	2.7726	.0286+ .0308-	•8120- •8791-	.0137-		•5246- •4670-
100	16	94	60.00	10.00	42.20	60.03	8.68	2.6672	-0359-	9454-	.0126-		•3196-
100	16	95	60.00	10.00	63.30	60.24	8.70	2.7646	.6436-		.0107-		.1651-
100	16	96	60.00	10.00	105.50	60.67	8 • 74	2.7195	•0453-		.0117-		•1977-
100	17	97	70.00	10.60	16.13	69.88	9.40	2.7005	-0261-	.8327-	-0161-	-0805-	•3760-
100	17 17	98 99	70.00	10.00	21.50	69.94	9.40	2.7614	•0312-	.9497-	•0162-	•1261-	•4472-
100	17	100	70.00	10.00	32.25 43.00	70.05 70.15	9•41 9•41	2.7866 2.7698	.0350- .0342-	1.0716- 1.1128-	•0166- •0154-	•0433- •0528	.2892- .1616-
100	18	103	80.00	10.00	16.22	80.03	9.85	2.9235	-0158-	1.1496-	.0121-	•0188	-2990-
100	18	104	80.00	10.00	21.62	80.09	9.85	2.9258	.0225-	1.1813-	.0123-	-0457	•2363-
100 100	18	165	80.00	10.00	32.43	80.19	9.85	2.7685	.6253-	1.1988-	•0127-	.0421	-2205-
100	18 18	106 107	80.00	10.00 10.00	43.24 64.86	80.29 80.52	9 • 8 6 9 • 8 6	2.7517	.0216- .0317-	1.2742- 1.3343-	.0140-	•0205 •0324	•2378- •2171-
100	18	168	80.00	10.66	108.10	81.00	9.88	2.8750	· ¢386-	1.4137-	.0150-	.0614	.1780-
100	19	109	96.00	10.00	16.28	90.17	10.00	2.8797	.0170	1.6486-	.0071-	•U218	.3409~
100	19	110	90.00	10.00	21.70	90.23	10.00	2.8496	.0103	1.6496-	-0073-	.0215	-2988-
100	19 19	111	90.00 90.00	10.60	32.55	90.32	10.00	2.7309	•6011-	1.6233-	.0073-	0405	2521-
100	19	112	90.00	10.00 10.00	43.40 65.10	90.44	10.00	2.7167	.0099- .0224-	1.6633- 1.7826-	.0077- .0091-	.0426 .0634	•2536- •2194-
100	19	114	90.00	10.00	108.50	91.05	10.00	2.6148	.0261-	1.6725-	.0081-	.0540	1894-
100	20	115	10.00	20.00	15.00	9.43	3.41	.6449	•0358	-1624-	-1د00.	•0266	.0787-
100	20	116	10.00	20.00	20.00	9.44	3.42	•6370	+0365	-1553-	.0026-	•0283	-دده٥٠
100	20	117 118	10.00	20.00 20.00	30.00 40.00	9.46 9.49	3.43 3.43	.6552 .6698	.0341 .0334	•1628- •1696-	•0029-	•0290	-0884-
100	20	119	10.00	20.60	60.00	9.53	3.45	-6828	.0326	.1784-	.0029-	+0291 +0285	-0899-
100	20	120	10.00	20.00	100.00	9.63	3.48	.7027	•0319	1844-	.0029-	.0271	.0862-
100	21	121	20.00	20.00	15.00	18.95	6.74	1.3268	.0295	.4548-	.0022-	•0170	-1545-
100	21 21	122 123	20.00	20.00	20.00	18.97	6.74	1.3566	-0277	•4806-	.0018-	•0133	-1424-
100	21	124	20.00	20,00	30.00 40.00	19.01 19.06	6 • 76 6 • 78	1.3379	.0263 .0257	•4784- •4819-	.0014-	•0120 •0118	•1412- •1371-
100	21	125	20.00	20.60	60.00	19.16	6.81	1.3743	.0250	.4939-	.0014	•0093	.1344-
100	21	126	20.00	20.00	100.00	19.35	6.87	1.4091	.0237	•5030-	.0023	-0068	-6د د 1 -
100	22	127	30.00	20.00	15.16	28.59	9.88	2.1589	.0081	.7379-	.0163-	.0242-	-60د
100	22	128	30.00 30.00	20.00 20.00	20.21 30.32	28.63 28.69	9.89 9.91	2.1259	•0095	•7605-	.0124-	•0307-	-1255-
100	22	130	30.00	20.00	40.42	28.77	9.93	2.1206	•0092 •0076	•7939- •8100-	-0033-	•0220- •0220-	•1457- •1668-
100	22	131	30.00	20.00	60.64	28.93	9.98	2.1601	0052	.8315-	.0034-		.1933-
100	22	132	30.00	20.00		29.22		2.1727	•0027	.8268-	.0014	•0453-	
100 100	23 23	133 134	40.00 40.60	20.00	15.34 20.45		12.73	2.4009 2.7347	-دد103 -1159-	•6631- •8492-	.0210- .0164-	•1303- •1345-	•1509- •0512-
100	24	139	50.00	20.00				l					
100	24	140	50.00	20.00	15.57 20.76		15.22 15.23	2.3621 2.2890	.0039 .0113	•5569- •6361-	.0256- .0143-	•2084~ •1800-	•3422- •3157-
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 $^{^{\}dagger}\text{Minus signs}$ are to the right of the numbers to which they apply.

TABLE III. - AERODYNAMIC COEFFICIENTS OF MODEL FOR THE COMPLETE INVESTIGATION - Continued

100 26 149 10 10 10 10 10 10 15 10 9 40 3 42 10 40 10 40 40 40 40 40	Config.	Run	Point	α ₁ , deg	ø, deg	q, lb/sq ft	α, deg	β, deg	c _N	CA	C _m	c1	Cn	C Y
10	100	25	145	66.00	20+60	15.83	58+54	17.45	1.8888	-0409-	•4086-	-0208-	-1090-	-807
00	100	26	149	10.00	20.00-	15.00	9.46	3.42-			-4010-		•0531-	.0604
1	100													•07∠9
100 26 153 10.00 20.	100													.0783
100	100													
00 27 156 20.00 20.00 20.00 20.00 20.00 20.00 20.00 27 157 20.00 20.00 27 158 20.00 20.00 27 158 20.00 20.00 20.00 20.00 20.00 27 158 20.00 20.0	100													.0803
00 27 158 20.00 20.00 30.00 19.03 6.77 1.5657 1.229 9.971 0.0069 1.221 1.22 1.22 1.22 1.22 1.22 1.22 1.	100													-1241
00 27 158 20.00 20.00 40.00 19.07 6.81 1.4587 1.3246 .9.461 .0071 2.203 1.215 00 27 160 20.00 20.00 19.36 6.868 1.4598 .0.34 .5259 .0.405 .0.177 1.215 00 28 161 30.00 20.00 20.00 19.36 6.868 1.4602 .0.234 .5259 .0.405 .0.1719 .1.215 00 28 162 30.00 20.00 20.00 20.00 19.36 6.868 1.4602 .0.234 .5259 .0.405 .0.1719 .1.215 00 28 163 30.00 20.00 20.00 20.00 19.36 6.868 1.4602 .0.234 .5259 .0.405 .0.1719 .1.215 00 28 165 30.00 20.	100													1266
19											1			
00 27 160 20.00 20.00 19-36 6.88 11-4602 .0234 .5299 .0044 .1119 .121 00 28 161 33.00 20.00 19-36 .988 1-4602 .0234 .5299 .0045 .1119 .121 00 28 163 30.00 20.00 20.10 .2014 .9886 .998 .24950 .0063 .9172 .0074 .0072 .122 00 28 164 30.00 20.00 .2014 .022 .2877 .992 .24930 .0063 .9172 .0094 .0092 .122 00 28 165 30.00 20.00 .2014 .022 .2877 .992 .24930 .0063 .9172 .0094 .0092 .122 00 28 166 30.00 20.00 .2014 .022 .2877 .992 .2407 .0068 .9413 .0029 .2122 .120 00 28 166 30.00 20.00 .2014 .022 .024 .10168 .24207 .0068 .9413 .0029 .2212 .120 00 29 167 4.000 20.00 .2014 .022 .024 .10168 .24208 .0032 .9467 .0033 .3355 .201 00 29 169 0.00 20.00 .2014 .022 .024 .10168 .24208 .0032 .9467 .0033 .3055 .201 00 29 170 40.00 20.00 .2016 .9824 .1274 .1274 .0032 .9821 .0072 .9921 .0076 .2014 .0070 .0090	100													1308
00	100							6.88-			•5299-		-6119-	•1275
100 28 163 30,00 20,00 30,32 28,71 9,92 2,3098 .0098 .9001 .0190 .0052 .121 .0020 .002	100									•0011				-1028
COD 28 164 30,000 22,000 40,02 28,179 994- 2,2407 4008 4817- 4012 CODA 23,100 20														
00 28 165 30.00 20.00 60.64 28.99 9.98- 2.2407 .0008 .99130029 .0212 .1210 00 29 167 40.00 20.00 15.34 38.40 12.74- 2.7214 .036581690123 .0772 .193 00 29 168 40.00 20.00 20.00 20.00 .315.34 38.40 12.75- 2.6707 .0122 .89960123 .0772 .193 00 29 170 40.00 20.00 .36.60 12.79- 2.4935 .000691400234 .0441 .12300230 .0230 .0231 .193 00 29 171 40.00 20.00 .36.60 12.79- 2.4935 .000691400234 .0441 .000 .029 .000 .029 .171 40.00 20.00 .102.25 39.74 .125- 2.4935 .000691400234 .0441 .000 .029 .000 .102.25 39.74 .125- 2.4935 .000691400234 .0441 .000 .029 .000 .102.25 39.74 .125- 2.4935 .000691400234 .0044 .000 .029 .000 .102.25 39.74 .125- 2.4935 .000691400234 .0044 .000 .000 .000 .000 .000 .000 .														
100 28 166 30.00 20.00 15.34 38.40 12.74 2.7214 .0365 .8169 .0123 .0335 .2030 .2	100													1561
100 29 168 40.00 20.00 30.48 38.44 12.75 2.4767 .0121 .8896 .0111 .0831 .134 .002 .004	100													•∠067
00 29 169 40.00 20.00- 30.68 38.53 12.77- 2.6413 0.002 .8921- 0.076 0.0719 .005 00 29 171 40.00 20.00- 61.55 38.60 12.79- 2.4935 0.006- 9149- 0.023 0.036 0.034 0.	100		167											•1987
00 29 170 40.00 20.00- 61.55 38.60 12.79- 2.4935 .000691490234 .0034 .0034 .0056 .00 29 172 40.00 20.00- 61.55 38.79 12.55 2.560 .0041- 19940994 .0161 .0056 .0061 .006100610061 .00610061 .0061	100													•1348
00 29 171 40.00 20.00 102.5 39.4 12.55 2.5603 .0041 .9934 .0359 .0561 .026 .000 .126 .	100			40.00					2.6413					•0093-
00				40.00										
1	100													.1224
100 30 175 50.00 20.00 31.15 48.51 15.25 2.5156 2.0047 8.741 0.0155 0.796 331 177 50.00 20.00 62.29 48.77 15.31 2.4624 0.085 8.844 0.0170 0.386 2.28 2.	100	30	173	50.00	20.00-	15.57	48.38	15.22-	2.7453		.7886-	•0198	-1827	.2749
10	100	30	174	56.60		20.76								-5209
00 30 177 50.00 20.00 103.82 49.17 15.31 2.4624 .0087 .8844 .0170 .0238 .287 .287 .24667 .0087 .9248 .0170 .0238 .287 .287 .008 .277 .0238 .287 .0238 .0243 .186 .600 .020 .2000 .277 .0238 .0243 .186 .600 .020 .2000 .277 .0238 .0243 .186 .600 .020 .2000 .271 .020 .020 .2000 .277 .0238 .0243 .186 .600 .020 .2000	100													-3015
10	100													•3386
1	100													.2741
1	100	21	170	60-00	20.00-	15-83	58.58	17-25-	2.6055	-0241-	-8698-	-0243	-1866	.6932
1	100													.6406
18	100													•67∠1
184	100													-6408
186	100 100													•4454
186	100	32	185	70.6u	20.60-	16.13	68.98	18.77-	2.6488	.0256-	.9189-	.026∪	.0445	•5517
18	100													•6599
189 70.00 20.00 107.50 69.41 18.87 2.5015 .0390 1.1723 .0269 .0662 .5010 .00314 .00	100													•6842
190	100													•5861
00	100 100													•5446 •5037
00	100	32	101	80.00	20.04-	16.22	79.54	19.69-	2.6570	.0314	1.3264-	.0192	.0605-	.4052
00 33 194 80.00 20.00- 43.24 79.77 19.71- 2.4426	100													-4154
00	100	33	193	80.00	20.00-	32.43	79.68							•4585
196	160													•4626
34	100 100													-4351 -4082
34	1:10	34	107	90 - Qu	20.00-	16.28	90.16	26.60=	2-6744	.5205	1.5016-	-0262	-0734-	.4262
00	130													.4434
00	100			90.00	20.00-		90.31	20.00-	2.5525	.0021		.0194		•4812
00	100													•4972
00	100 100													•4668 •4410
00		35		ł	30-111-			4.00-	ı	.0302	.1375-	.0059	.0350-	•1183
00 35 205 10.00 30.00- 30.00 8.73 5.01- .5966 .0362 .1479- .0057 .0368- .118 00 35 206 10.00 30.00- 60.00 8.74 5.02- .5982 .0354 .1511- .0059 .0375- .117 00 35 207 16.00 30.00- 60.00 8.78 5.02- .6208 .6351 .1607- .0057 .0390- .127 00 35 208 10.00 30.00- 10.00 8.85 5.08- .6365 .0351 .1655- .0059 .0390- .127 00 36 210 20.00 30.00- 17.55 9.88- 1.2215 .0286 .4160- .0023 .0320- .211 00 36 211 20.00 30.00- 30.00 17.60 9.990- 1.2431 .6273 .4388- .0019 .0320- .201 00 36 <	100												1 1 2 1	.1201
00 35 208 10.00 30.00- 60.00 8.78 5.04- 6.208 .0351 .16070057 .0375117 .00 35 208 10.00 30.00- 100.00 8.85 5.08- 6.365 .0351 .16070057 .0396121 .00 36 209 20.00 30.00- 15.00 17.55 9.88- 1.2175 .0286 .41600023 .0320211 .00 36 210 20.00 30.00- 20.00 17.60 9.88- 1.2275 .0286 .44320019 .0314199 .00 36 211 20.00 30.00- 30.00- 17.60 9.90- 1.2231 .0273 .43880019 .0320201 .00 36 212 20.00 30.00- 40.00 17.64 9.92- 1.2506 .0276 .44120010 .0321208 .00 36 213 20.00 30.00- 40.00 17.64 9.92- 1.2506 .0276 .44120010 .0321208	100		205	10.00		30.00	8.73	5.01-	•5966	.0362	•1479-	.0057	-0368-	.1186
00 36 210 20.00 30.00- 100.00 8.85 5.08- 6.365 .0351 .1655- 0.059 .0396- 1210.00 36 210 20.00 30.00- 20.00 17.56 9.88- 1.2629 .0283 .44320019 .0314- 1950.00 36 211 20.00 30.00- 30.00- 30.00- 17.60 9.990- 1.2431 .6273 .43880019 .03202010.00 36 212 20.00 30.00- 40.00 17.64 9.92- 1.2506 .6276 .44120010 .03212080.00 36 213 20.00 30.00- 60.00 17.71 9.996- 1.2618 .0256 .44270011 .03472130.00 36 213 20.00 30.00- 60.00 17.71 9.996- 1.2618 .0256 .44270011 .03472130.00 36 213 20.00 30.00- 60.00 17.71 9.996- 1.2618 .0256 .44270011 .03472130.00 30.00- 30.00- 60.00 17.71 9.996- 1.2618 .0256 .44270011 .03472130.00 30.00- 30.00- 60.00 17.71 9.996- 1.2618 .0256 .44270011 .03472130.00 30.00- 3	100													•1175
00 36 210 20.00 30.00- 20.00 17.55 9.88- 1.2175 .0286 .41600023 .0320211 .00 36 211 20.00 30.00- 30.00- 30.00 17.60 9.88- 1.2629 .0283 .44320019 .0320250 .00 36 211 20.00 30.00- 30.00 17.60 9.90- 1.2431 .0273 .43880019 .0320250 .00 36 212 20.00 30.00- 40.00 17.64 9.92- 1.2506 .0276 .44120010 .03212080 .00 36 213 20.00 30.00- 60.00 17.71 9.96- 1.2618 .0256 .44270011 .0347213	100 100													•1∠00 •121i
00 36 210 20.00 30.00- 20.00 17.56 9.88- 1.2629 .0283 .44320019 .0314195 00 36 211 20.00 30.00- 30.00- 9.90- 1.2631 .0273 .43880019 .0320207 00 36 212 20.00 30.00- 40.00 17.64 9.92- 1.2506 .6276 .44120010 .0321208 00 36 213 20.00 30.00- 60.00 17.71 9.996- 1.2618 .0256 .44270011 .0347213								l			4160-			
00 36 212 20.00 30.00- 40.00 17.64 9.92- 1.2506 .0276 .44120010 .0321208 00 36 213 20.00 30.00- 60.00 17.71 9.96- 1.2618 .0256 .44270011 .0347213	100	36	210	20.00	30.00-	20.00	17.56	9.88-	1.2629	.0283	•4432-	.0019	-0314-	•1998
00 36 213 20.00 30.00- 60.00 17.71 9.96- 1.2618 .0256 .44270011 .0347213	100												•6320-	•2073
	100							9.92-						
	100								1.2852					•2137
	100	اهد	214	20.00	50.00-	100.00	11.00	10.04-	105025	•0251	******	.0004-	.0320-	•2100
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 $^{^{\}dagger}$ Minus signs are to the right of the numbers to which they apply.

TABLE III. - AERODYNAMIC COEFFICIENTS OF MODEL FOR THE COMPLETE INVESTIGATION - Continued

Config.	Run	Point	α ₁ , deg	ø, deg	q, lb/sqft	α, deg	β, deg	C _N	C _A	C m	cı	Cn	CY
100	37 37	215 216	30.00 30.00	30.00- 30.00-	15•16 20•21	26.65 26.69	14.52-	1.9247	•0141 •0159	.6563− .7087~	.00UZ-	•0426 •0328	•2112 •2340
100	37	217	30.00	30.00-	30.32	26.74	14.56-	1.9419	0173	7190-	-0026-	•C278	-2340
100	37	218	30.00	30.00-	40.42	26.80	14.59-	1.8973	.0151	7256-	.0044~	•0z56	.2654
100	37	219	30.00	30.00-	60.64	26.91	14-64-	1.9274	.0147	7503-	-0013-	11د٥.	•3079
100	37	220	30.GU	30.00-	101.06	27.15	14.76-	1.9547	•0119	.7561-	•0040	28 د ۵۰	•3248
100	38	221	40.00	30.00-	15.34	36.12	18.80-	2.6133	.0166	•83∠3 -	•0379	•1010	.1464
100	38	222	40.00	30.60-	20.45	36.15	18.81-	2.5030	•C154	•8C97 -	•3373	•0878	.1392
100	38	223	40.00	30.00-	30.68	36.23	18.85-	2.4349	•C165	-6دَوٰ8٠	•0474	•0415	•1576
100	38	224	40.00	30.00~	40.90	36.31	18.88-	2.4210	•UU98	•8567-	•0504	8 660•	-1456
100	38 38	225	40.00	30•0u- 30•0u-	61.35	36.49 36.84	18.95-	2.5790	•6028 •0011-	1.0092-	.0678 .0840	+0824 +0941	•2578 •3050
	٥٥	226			102.25	30+04	19.10-	2.6488	•0011-	1.0367-		10941	
100	39	227	50.00	30.00-	15.57	46.02	22.57-	2.4909	•0164	-8756-	.0276	•0865	دد 480
100	39	228	50.00	30.00-	20.76	46.06	22.58-	2.4319	•6150	•8093- •7432-	0304	0539	•4586
100	39 39	229 230	50.00 50.00	30.00- 30.00-	31.15	46.13 46.21	22.60-	2.3251	•01.55 •0693	•7432- •8522-	•0294 •0266	•0055- •0242+	•4673 •4109
100	39	231	50.00	30.00-	62.29	46.38	22.69-	2.3434	.0026	•9500-	.0298	•0075	•4346
100	39	232	50.Cu	30.00-	103.82	46.67	22.79-	2.2676	.6018-	•9096-	.0256	•0239-	•4735
100	40	233	60.00	30.00-	15.83	56.44	25.69-	2.3106	.0399-	•8134-	41 د 0 ه	•1479	.8085
100	40	234	60.00	30.00-	21.10	56.47	25.70-	2.2799	-0384-	.8492-	.0302	•1336	7814
100	40	235	60.00	30.60-	31.65	56.56	25.73-	2.2666	•0349-	•9689-	.0276	•1269	•7981
100	40	236	60.00	30.00-	42.20	56.65	25.75-	2.3340	•6317-	.9754-	.0264	•6558	د 689ء
100	40	237	60.00	30.00-	63.30	56.8∪	25+79-	2.2681	•6302-	•952U-	.0272	.0043-	-6148
100	40	238	60.00	30.00-	105.50	57.15	25.88-	2.3335	•0418-		.0321	•0432-	•5953
100	41	239	70.00	30.00-	16•13	67.33	28.05-	2.3178	•0256-	.9494-	.0280	•0820	4د70ء
100	41	240	70.00	30.66-	21.50	67.37	28+06-	د2228ء	•0317-	1.1002-	•0249	•1544	• 7900
100	41	241	70.00	30.00-	32.25	67.44	28.07-	2.1712	•0269~	1.1844-	.0256	•1381	•7538
100	42	245	80.00	30.00-	16.22	78.65	29.51-	2.4306	.0281	1.2462-	.0347	•0971-	-616∠
100	42	246	80.00	30.00-	21.62	78.68	29.52-	2.3678	.0243	1.2294-	.0342	•0898-	-5971
160	42	247	80.00	30.00-	32.43	78.77	29.53-	2.2824	•0028	1.3613-	•0340	•0257-	•6979
100	42	248	80.00	30.00-	43.24	78.84	29.53-	2.1576	•0042	1.3445-	1 د د ن ٠	• 0245-	•6714
100	42	249	80.00	30.60-	64.86	79.03	29.55-	2.2498	•¢096-	1.3490-	•0355	•1021-	.5829
100	42	25↓	80.00	30.00-	108.10	79.39	29.58-	2.2634	•0114-	1.3802-	•0204	•1037-	•6221
100	43	251	90.00	30.00-	16.28	90.15	30.00-	2.4979	•0300	1.3968-	.0379	•1385-	-5684
100	43	252	90.00	30.00-	21.70	90.20	30.00-	2.3808	•0208	1.3682-	.0377	•1277-	•5841
100	43	253	90.00	30.cu-	32.55		30.00-	2.2787	•0068	1.4635-	•0351	.1024-	-6147
100	43	254 255	90.00 90.00	30.00- 1 30.00-	43.40	90.36	30-00-	2.1995	•0058-	1.4428-	.0352	•0893-	•6305
100	43	256	90.00	30.00-	65.10 108.50	90.53	30.00- 30.00-	2.2075 2.1887	•0200- •0299-	1.4476-	.0344 .0346	•1350- •1342-	•5834 •6230
.00	44	257	10.60	40.00-	15.00	7.70	6.42-	•5864	•0285	•1667-	•0043	•0581-	11.56
100	44	258	10.00	40.00-	20.00	7.71	6.42-	•5686	•0283 •0283	•1624-	.0043	+0569-	•1589 •1649
100	44	259	10.60	40.00-	30.00	7.73	6.44-	•5497	0277	1522-	.0042	•0576-	1656
100	44	260	10.00	40.00-	40.00	7.73	6.44-	-5535	.0288	1525-	.0036	•0576-	1660
100	44	261	10.00	40.00-	60.00	7.76	6.47-	•5596	.0293	-1508-	.0048	·0586-	•1702
100	44	262	10.00	40.00-	100.00	7.81	6.51~	•5599	•0299	-1508-	•0049	•0582-	•1683
100	45	263	20.00	40.60-	15.00	15.61	12.73-	1.1156	•0143	.3941-	•0079	•0822-	•3339
100	45	264	20.00	40.00-	20.00	15.62		1.1352	.0163	.3953~	.0082	•0852-	•3496
100	45		20.00	40.00-	30.00	15.66		1.1221	.0169	•3942-	.0064	-8080-	•3353
100	45		20.00	40.00- 40.00-	40.00 60.00	15.68		1.1029	•U168	•3876− •3920−	.0055	•0785-	*3306
00	45		20.00	40.00-	100.00	15.73 15.83		1.1045	•0165 •0172	•3920 -	.0051 .0039	•0776- •0734-	•3274 •3224
.00	46	269	30.00	40.00-	15.16	23.93		1.7502	•0616	•6445-	•000>	•0348-	4 - 26
100	46	270	30.00	40.00-	20.21	23.95		1.7857	.0014	6746-	.0032-	•0348- •0278-	•4529 •4655
00	46	271	30.00	40.00-	30.32	23.99		1.6861	0007	.6>8U~	.0056-	•9181-	4556
.00	46	272	30.00	40.00-	40.42	24.02		1.6504	-0008-	•6705-	.0067-	•0230+	•4693
00	46	273	30.00	40.00-	60.64		18-91-	1.6453	.0008	.6697-	.0007	.0251-	•4710
00	46	274	30.00	40.00-			19.02-	1.6504	•0021	•6695-	.0003	.0170-	•4729
100	47	275	40.00	40.60-	15.34			2.1546	.0034-	•7545-	.0695	•C284	•4979
100	47	276	40.00	40.00-	20.45			2.2117	•UU5U-	.8045-	.0690	•0135	•5007
.00	47		40.00	40.00-	30.68			2.2726	•0062-	8586-	•0751	•0218	•49∠6
UO .	47		40.00	40.60-	40.90			2.2482	•0085-	•8839-	.0810	•0154	•516i
100	47		40.00	40.00-	61.35 102.25	33.09 33.34		2.2694 2.2747	•0089- •0164-	•9374- •9835-	.0961 .0943	.0023 .0355	•5430 •5767
JU			50.00	1	l								
.00	48 48		50.00	40.66- 40.66-	15.57 20.76	42.50 42.53		2.3509 2.2465	•0224- •0166-	.7936- .7191-	•0298 •0275	•\$231- •\$614-	•534∠ •4851
100	48		50.00	40.00-				2.2264	•0166- •0127-	.7885~	.0259	•0496-	•4851 •5062
00	48		50.00	40.00-	41.53			2.1060	0101-	7812-	•026U	.0531-	•5224
00	48		50.00	40.00-	62.29	42.79		2.2195	.0168-	.8916-	.0390	•0421-	•5281
00	48	286	50.00	40.60-		43.02		2.0822	.0176-	•853C−	.0335	.0297-	•6037
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 $^{{}^{\}dagger}\text{Minus signs}$ are to the right of the numbers to which they apply.

TABLE III. - AERODYNAMIC COEFFICIENTS OF MODEL FOR THE COMPLETE INVESTIGATION - Continued

Config.	Run	Point	α ₁ , deg	ø, deg	q, lb/sqft	a, deg	β, deg	C _N	C _A	C _m	c¹	Cn	С¥
100	49	287	10.00	50.00-	15.00	6.47	7.66-	.4658	•6274	•107ž-	-0046	•0709-	•1914
100	49	288	10.00	50.00-	20.00	6.47	7.66-	.4504	-0290	-1105-	.0043	-0712-	1905
100	49	289	10.00	50.00-	30.00	6.48	7.66-	.4536 .4483	.0279 .0290	•1188- •1099-	.0041 .0043	•0679- •0698-	•1888 •1951
100	49	290	10.00	50.00-	40.00	6.49	7.69-	.4548	.0301	.1131-	.0044	•0725-	1996
100 100	49	291 292	10.00	50.00-	100.00	6.53	7.72-	.4682	.0304	.1202-	.0044	.0736-	.2010
100	50	293	20.00	50.00-	15.00	13.18	15.21-	.9107	.0138	•3017-	.0157	-1449-	•4647
100	50	294	20.00	50.00-	20.00	13.19	15.22-	.8886	•0148	•2905- •2904-	.0137 .0129	•1413- •1362-	•4570 •4546
100	50	295	20.60	50.00-	30.00 40.00	13.20	15.23-	.8842 .8619	.0147 .0139	.2792-	.0126	1305-	.4413
100	50 50	296 297	20.00	50.60-	60.00	13.25	15.29-	.8831	.0144	.2908-	.0141	.1306-	•4458
100	50	298	20.00	50.00-	100.00	13.31	15.34-	.8923	•0149	.2932-	.0118	•1261-	•4400
100	51	299	30.00	50.00-	15.16	20.40	22-56-	1.3587	.0001-	-5140-	.0251	● 1671-	-7132
100	51	300	30.00	50.00-	20.21	20.41	22.57-	1.3851	.0017-	•5413- •5390-	.0207 .0142	•1603- •1466-	•7054 •6821
100	51 51	301 302	30.00 30.00	50.00-	30.32 40.42	20.44	22.62-	1.3568	-0044-	-5655-	.0079	1397-	.7047
100	51	302	30.00	50.00-	60.64	20.51	22.67-	1.3644	-0065-	.5858-	-0046	•1344-	•7279
100	51	304	30.00	50.00-	101.06	20.60	22.75-	1.3473	•0063-	•5816-	•0062	•1301-	.7188
100	52	305	40.00	50.00-	15.34	28.40	29.55-	1.7973	.0134-	•7161-	•0972	•1630-	•8908 •9194
100	52	306	40.00	50.00- 50.00-	20.45 30.68	28.42 28.45	29.56- 29.59-	1.8359	•0086- •0124-	•7665- •7522-	•1057 •1024	•1638- •1576-	8786
100	52 52	307 308	40.00	50.00-	40.90	28.49	29.62-	1.7550	.0118-	.7704-	.1039	•1559-	.8777
100	52	309	40.00	50.00-	61.35	28.56	29.68-	1.7582	.0127-	.8338-	•0983	-1546-	•9120
100	52	310	40.00	50,60-	102.25	28.70	29.78-	1.7067	•0169-	.8594-	-0895	•1222-	•9479
100	53	311	10.00	60.00-	15.00	5.04	8.65-	.3459	•0370	•0829−	•0045	·C879-	-2386
100	53	312	10.00	60.00-	20.00	5.04	8.65-	.3745	.0357	•0979-	•00∠1	•0909-	•2501
100	53	313	10.00	60.00-	30.00	5.04	8.66-	•3329	.0336	.0834- .0883-	•9026 •9025	•0834- •0852-	•229 · •2311
100	53	314 315	10.00	60.00-	60.00	5.05	8.67-	•3449 •3560	.0336	.0928-	.0023	-0869-	.2352
100	53	316	10.00	60.00-	100.00	5.06	8.70-	.3467	.0331	.0862-	•0029	•0854-	•2304
100	54	317	20.00	60.00-	15.00	10.32	17.25-	.6642	.0153	-2122-	•0116	•1909-	•5564
100	54	316	20.00	60.00-	20.00	10.32	17-26-	.6886	•0161	•2229-	.0110	•1911-	•5596
100	54	319	20.00	60.00-	30.00	10.33	17-26-	-6878	.0158 .0150	•2222- •2105-	•0108 •0101	•1865- •1813-	•5569 •5438
100	54 54	320	20.00	60.00-	60.00	10.34	17.27- 17.29-	•6617 •6651	.0149	.2113-	.010C	.1817-	-5491
100 100	54	321 322	20.00	60.00-	100.00	10.38	17.34-	.6759	.0171	.2167-	.0054	•1811-	•5530
100	55	323	30.00	60.00-	15-16	16.12	25.69-	.9671	.0034	•3779-	.0235	-2528-	.8521
100	55	324	30.00	60.00-	20.21	16.12	25.69-	1.0028	96000	-4023-	-0236	-2530-	-8436
100	55	325	30.00	60.60-	30.32	16.14	25.71-	1.0102	.0036	.4239-	0206	•2523-	.8612 .8432
100	55	326	30.00	60.00-	40.42	16.14	25.72- 25.75-	.9705 .9699	.0041 .0001-	•4174- •4300-	•0179 •0108	•2443- •2408-	-8523
100 100	55 55	327 328	30.00 30.00	60.60-	101-06	16.17 16.21	25.81-	.9768	.0013	•4379-	.0119	•2382~	.8587
100	56	329	40.00	60.00-	15.34	22.79	33.86-	1.3148	.0114-	-5465-	•0911	•2844-	
100	56	330	40.00	60.00-	20.45	22.80	33.87-	1.2733	-8600	•5378-	.0867	•2986-	
100	56	331	40.00	60.00-	30.68	22.81	33.88-	1.2387	.0031-	•5604-	.0906	-2969-	1.0639
100	56	332	40.00	60.00-	40.90	22.83	33.90- 33.94-	1.2130	.0063 .0020	•5954- •6423-	.0915 .0958	•3006- •3036-	1-1203
100	56 56	333 334	40.00	60.00-	61.35 102.25	22.86	34.02-	1.2608	.0007-	-6705-	-1028	•2961-	
100	57	335	5.00	70.00-	15.00	1.71	4.70-	.1611	.0428	.0497-	-0005	•0536-	•1270
100	57	336	5.00	70.00-	20.00	1.71	4.70-	-1578	.0424	.0478-	•0006	-0512-	•1193
100	57	337	5.00	70.00-	30.00	1.71	4.70-	•1377	-0440	.0365- .0390-	•0006 •0006	•0511- •0499-	•1219 •1200
100	57	338	5.00	70.00-	40.00 60.00	1.71	4.70- 4.70-	•1279 •1225	.0397 .0416	.0333-	•0006	•0497-	.1224
100	57 57	339 340	5.00	70.00-	100.00	1.72	4.71-	.1236	.0411	.0317-	•0006	-0479-	.1210
100	58	341	10.00	70.00-	15.00	3.45	9.39-	.2442	•0375	.0689-	•0006	•1005-	•2549
100	58	342	10.00	70.00-	20.00	3.45	9.40~	.2450	-0377	.0659-	-0011	•1021-	•2626
100	58	343	10.00	70.00-	30.00	3.45	9.40-	•2467	.0371 .0370	.0702-	.0015 .0017	•0959- •0966-	•2495 •2507
100	58	344 345	10.00	70.00-	60.00	3.45	9.40-	.2344 .2358	.0370	.0639-		•0954-	·2496
100	58 58	346	10.00	70.00-	100.00	3.46	9.42-	.2358	.0365	.0617-		-0955-	•250C
100	59	347	20.00	70.00-	15.00	7.09	18-76-	4908	-0162	.1788-		•2545-	•6555
100	59	348	20.00	70.00-	20.60	7.09	18-76-	•4560	-0158	•1667- •1669-		•2439- •2393-	•6292 •6242
100	59 59	349 350	20.00	70.00-	30.00 40.00		18.77~ 18.77~	.4458 .4540	.0162 .0163	•1673-			.6332
100	59	350	20.00	70.00-	60.00		18.78-	.4452	.0170	-1595-			•6394
106	59	352	20.00	70.00-	100.00		18.80-	.4436	.0171	.1592-			•6320
100	60	353	30.60	70.00-	15-16	11.17	28.04-	•5778	•0075	-2364-		+3036~	•9279
100	60	354	30.00	70.00-	20.21		28.05~	•6090	•0084	•2628-		•3171-	•9373 •9234
100	60	355	30.00	70.00-	30.32		28.05- 28.05-	•5966 •5806	.0096 .6097	•2719- •2728-		•3145- •3074-	.9234
100	60	356 357	30.00 30.00	70.00-	60.64	11.16	28-06-	-5715	.0097	.2776-		•3084-	.9238
100	60	358	30.00	70.00-	101.06	11.20	28-09-	-5604	0096	.2794-	.00>3	•3010-	.9241
			L	L		L	<u> </u>		L		L	<u> </u>	L

 $^{^{\}dagger}$ Minus signs are to the right of the numbers to which they apply.

TABLE III. - AERODYNAMIC COEFFICIENTS OF MODEL FOR THE COMPLETE INVESTIGATION - Continued

Config.	Run	Point	α ₁ , deg	g, deg	q, lb/sq ft	α, deg	β, deg	c _N	C _A	C _m	c,	Cn	С¥
100	61	359	40.00	70.00-	15.34	16.01	37.17-	.7664	.0106	•3136-	-0644	•3411-	
100	61	360	40.00	70.00-	20.45	16.02	37-18-	7295	-0161	•3177-	0546	•3496-	
100	61	361	40.00	70.00-	30.68	16.03	37.19-	•7485	•6191	-3810-	•0496	•3456 -	
100	61	362	40.00	70.00-	40.90	16.03	37.19-	.6369	.0212	+3483-	.0488	•3250-	
100	61	363	40.00	70.00-	61.35 102.25	16.03	37.20- 37.22-	•5285 •5485	.0216 .0224	•3311- •3285-	.0531 .0551	•3173- •3192-	
100	61	364	40.00						1				
100 100	62 62	359 360	5.00 5.00	80.00-	15.00 20.00	.87: .87	4.92-	.0804 .0859	.0431	.0175- .0234-	.0015- .0010-	•0658- •0597-	•1713 •1605
100	62	361	5.00	80.00-	30.00	.87	4.92-	0803	0432	0243-	0005-	0595-	.1506
100	62	362	5.00	80.00-	40.00	.87	4.92-	0725	0433	0200-	-0006-	.0554-	1411
100	62	363	5.00	80.00-	60.00	.87	4.92-	.0641	.0424	.0173-	.0004-	.0537-	•1371
100	62	364	5.00	80.00-	100.00	.87	4.92-	.0655	•0425	.0165-	-0002-	•0518-	•1336
100	63	365	10.00	80.00-	15.00	1.75	9.84-	.1464	.0397	.0407-	•0015-	•1132-	
100	63	366	10.00	80.00-	20.00	1.75	9.84-	.1467	.0394	.0409-	.0012-	•1C71-	
100	63	367	10.00	80.00-	30.00	1.75	9 - 84-	•1385	.0396	. 0403-	.0010-	-1045-	
100	63	368	10.00	80.00-	40.00	1.75	9.84-	.1280	.0394	•0355-	.0008- .0005-	•1028-	•2699
100	63	369	10.00	80.00-	60.00	1.75	9 • 84-	.1214	.0398 .0393	.0335- .0337-	.0003-	•1030- •1010-	•2687 •2628
100	63	370	10.00	80.00-	100.00	1.75	9.85-	.1214					
100	64	371	20.00	80.00-	15.00	3.61	19.69-	.2381	±0255	•0986-	+0087-	•2855-	•6973
100	64	372	20.00	80.00-	20.00	3.61	19.69-	•2528	.0238	•1108-	+0087-	•2751-	•6709 •6703
100	64	373	20.00	80.00- 80.00-	30.00	3.61 3.61	19.69-	•2236 •2171	•0247 •0239	•0972- •0969-	.0081- .0083-	•2729- •2642-	•6540
100	64	374 375	20.00	80.00-	40.00 60.00	3.61	19.69-	2090	.0239	.0909-	.0084-	•2666-	.6645
100	64	376	20.00	80.00-	100.00	3.61	19.69-	.2051	.0239	.0881~	-0085-	•2675+	.6697
100	65	377	30.00	80.00-	15.16	5.72	29.50-	.2503	.0249	.1048-	.0082-	•3515-	1.0130
100	65	378	30.00	80.00-	20.21	5.72	29.50-	.2551	.0263	.1156-	-0095-	-3590-	-9652
100	65	379	30.00	80.00-	30.32	5.72	29.50-	.2400	.0247	.1324-	-0098-	•3730-	.9795
100	65	380	30.00	80.00-	40.42	5.72	29.51-	.2327	.0232	•1507-	.0121-	•3657-	.9712
100	65	381	30.00	80.00-	60.64	5.72	29.51-	.2088	.0240	•1583~	•0147-	•3642-	•9859
100	65	382	30.00	80.00-	101.06	5.72	29.51-	·1692	•0233	.1386-	•0170-	•3475-	•9656
100	66	383	40.00	80.00-	15.34	8.29	39.27-	.2730	.0237	.0999-	•0296	•3394-	
100	66	384	40.00	80.00-	20.45	8.29	39.27-	.2554	.0293	.0826-	•0194	•3388-	
100	66	385	40.00	80.00-	30.68	8.29	39.27-	.2250 .1884	.0336	•1112- •1525-	•0128 •0040	•3550- •3536-	11 - 1526
100	66	386	40.00	80.00- 80.00-	40.90	8.29	39.27- 39.27-	.1220	.0308 .0288	.2126-	•0016	•3594~	
100 100	66	387 388	40.00	80.00-	102.25	8.29	39.28-	0975	.0306	.2001-	.0017	-3592-	
				20.00		6.0	3 60	.0282	.0458	.0130-	.0012	•0293-	.0553
100	67	389 390	2.50	90.00-	15.00	00	2.50-	.0204	.0457	.0093-	0004	.0250-	.0421
100	67	400	2.50	90.00-	30.00	.00	2.50-	.0123	.0444	.0122-	.0006	.0276-	.0557
100	67	401	2.50	90.00-	40.00	.00	2.50-	.0100	.0441	.0075-	.0004	.0241-	.0574
100	67	402	2.50	90.00-	60.00	.00	2.50-	.0053	.0445	-0082 -	.00Q2.	-0257-	.0580
100	67	403	2.50	90.00-	100.00	•00	2.50-	.0079	•0446	.0083-	.0001-	•0246-	.0593
100	68	404	5.00	90.00-	15.00	.00	5.00-	.0057~	•0461	.0034	•0006	.0527-	•1303
100	68	405	5.00	90.00-	20.00	.00	5.00-	•0051-	•0467	.0031	.0002 .0003-	•0523-	.1303 .1304
100	68	406	5.0u	90.00-	30.00	.00	5.00-	.0043	.0427	.0021- .0017	.0000	.0518- .0484-	.1222
100	68	407	5.00	90.00-	60.00	.00	5.00-	.0086	.0443	.0052-	-0004-	-0493-	.1225
100	68	409	5.00	90.00-	100.00	.00	5.00-	.0035	.0439	.0058-	.0005-	•0501-	.1244
100	69	410	7.50	90.00-	15.00	.00	7.50-	.0065-	.0442	.0041	.0005-	.0745-	.1849
100	69	411	7.50	90.QU-	20.00	.00	7.50-	.0064-	.0463	.0041	-0009-	-0786-	-1958
100	69	412	7.50	90.00-	30.00	.00	7.50-	.0033	.0441	.0027-	.0011-	•0769-	1958
100	69	413	7.50	90.60-	40.00	.00	7.50-	.0075	•0443	.0057-	.0010-	•0757-	-1918
100	69	414	7.50	90.00-	100.00	.00	7.50- 7.50-	.0033	.0434	.0034-	.0011-	•0748- •0753-	1904
		i	1		1		Į.						
100	70	416 417	10.00	90.00-	15.00	.00	10.00-	.0078- .0069-	.0468 .0451	.0050 .0046	.0012-	1065-	•2715 •2612
100	70		10.00	90.00-	30.00		10.00-	.0107	.0426	.0093-	.0023-	1030-	.2615
100	70	419	10.00	90.00-	40.00		10.00-	.0065	.0417	.0060-	.0023-	-1017-	•2574
100	70	420	10.00	90.00-	60.00	.00	10.00-	.0109	.0424	.0087-	.0024-	+1026-	2589
100	70	421	10.00	90.00-	100.00	•00	10.00-	.0012	.0414	.0041-	•0020-	•1013-	.2580
100	71	422	15.00	90.00-	15.00	•00	15.00-	.0113-	.0423	.0023	.0050-	-1735-	.4259
100	71	423	15.00	90.00-	20.00	•00	15.00-	.0105-	.0428	.0012	•0059-	•1716-	.4183 .4156
	71	424	15.00	90.00-	30.00	•00	15.00-	.0083 .0094-	.0397	.0141-	.0057- .0054-	•1670- •1647-	4097
100	71	425	15.00	90.00-	60.00	.00	15.00-	0052-	.0383	.0025-	0055-	1695-	4232
100	1 / 1	426 427	15.00	90.00-	100.00	.00	15.00-	.0127-	.0376	.0009-	.0057-	1719-	.4261
	71				1	1	1	I	1	1	l .	ŀ	1
100 100 100		1	20 - 04	90-60-	15-00	-00	20.00-	.0166-	0355	.0125-	-16(0.1	-2814~	.6604
100 100 100	72	428	20.00	90.00-	15.00	•00	20.00-	.0166-	.0355 .0338	.0125- .0121-	•0131- •0135-	•2814- •2814-	.6504
100 100 100 100	72 72	428 429	20.00	90.00-	20.00	.00	20.00-	.0166- .0173- .0146-	.0355 .0338 .0320	.0121- .0162-	.0135- .0142-	•2814- •2779-	•6548 •6555
100 100 100	72	428		90.00- 90.00- 90.00-	20.00 30.00 40.00	.00	20.00-	.0173- .0146- .0200-	.0338 .0320 .0307	.0121- .0162- .0155-	.0135- .0142- .0144-	.2814- .2779- .2726-	.6548 .6555
100 100 100 100 100 100	72 72 72	428 429 430	20.00	90.00-	20.00	.00	20.00-	.0173- .0146-	.0338 .0320	.0121- .0162-	.0135- .0142-	•2814- •2779-	•65∠8 •6555

 $[\]dagger_{\mbox{Minus signs}}$ are to the right of the numbers to which they apply.

TABLE III. - AERODYNAMIC COEFFICIENTS OF MODEL FOR THE COMPLETE INVESTIGATION - Continued

	1		T	Т	T				T	1 -	Τ	γ -	T
Config.	Run	Point	α ₁ , deg	ø, deg	q, lb/sq ft	α, deg	β, deg	C _N	C _A	C _m	Cl	Cn	С¥
100 160	73 73	434	25.00	90.00-	15.00	.00	25.00-	.0584-	.0353	.0046-			-8558
100	73	436	25.00	90.00-	30.00	.00	25.00-	.0613-	.0357 .0336	.0023- .014>-	.0225-	•3508- •3581-	-8505
100	73	437	25.00	90.00-	40.00	.00	25.00-	0702-	.0323	.0051-	0257-	•3470-	-8662 -8399
100	73	438	25.00	90.00-	60.00	.00	25.00-	.0809-	.6325	0045-	.0259-	-3455-	.8489
100	73	439	25.00	90.66-	100.00	.00	25.00-	.1054-	.0306	.0014-		•3404-	.8500
100	74	440	30.00	90.00-	15.16	.00	30.00-	.1000-	.0342	.0382	.0152-		.9540
100	74	441	30.00	90.00-	20.21	.00	30.00-	.1292-	.0383	.0560	•0176-		•9831
100 100	74 74	442	30.00 36.06	90.00-	30.32	.00	30.00-	.0985- .1038-	•0371 •0347	.0192 .0034-	.0231-	•3783-	•9695
100	74	444	36.00	90.00-	60.64	.00	30.00-	1408-	.6321	.0062-	•0270- •0318-	•3835- •3930-	•9713 •9984
100	74	445	30.00	90.00-	101.06	•00	30.00-	•1557-	•0306	-0096-		-3851-	
100	75	446	40.00	15.00-	15.34	39.18	9.61-	2.9298	.0521-	.8125-	.0556	•0685	-1680
100	75	447	40.00	15.00-	20.45	39.23	9 • 62 -	2.8506	-0408-	.8516-	.0325	.0619	-1516
100	75	448	40.00	15.00-	30.68	39.33	9.64-	2.7864	.6231-	•9375-	.0140	•0599	•0374-
100	75 75	449 450	40.00	15.00-	40.90	39.40	9.65-	2.6119	.0220-	•9412-	•0291	•0451	•0043-
100	75	451	40.00	15.00-	61.35 102.25	39.99	9.69- 9.77-	2.5969	•0222- •0156-	•9849~ •9770-	.0365 .0153	•0385 •0721	•0114 •0275
100	76	452	50.00	15.00-	15.57	49.18	11.46-	2.8262	.0354-	•6552-	1		ļ
Ϊυο	76	453	50.00	15.00-	20.76	49.23	11.47-	2.8515	.0355-	1534-		•1720 •1772	•3631 •3148
100	76	454	50.00	15.00-	31.15	49.30	11.48-	2.5445	.0236-	8332-		•1163	-3640
100	76	455	50.00	15.00-	41.53	49.40	11.50-	2.5741	•0259-	-8839-		+1002	+3284
100	76 76	456 457	50.00	15.00- 15.00-	62.29 103.82	49.58	11.53-	2.5294	•0248-			•0768	•2767
					103.02	49.97	11.59-	2.5485	•0230-	•9137-	•0125	•0388	•2252
100	77	458	60.00	15-00-	15.83	59.49	12.97-	2.8517	•0432-	8946-	•0217	•2250	•6296
100	77	459	60.00	15.00-	21.10	59.34	12.98-	2.7287	•0476-	-8590-	+0186	•2148	•6158
100	77	460 461	60.00	15.00-	31.65 42.20	59.45 59.53	12.99- 13.00-	2.7352	.0539- .0513-	•9420-	•0194	•2130 •1598	•6531
100	77	462	60.00	15.00-	63.30	59.74	13.00-	2.6510	.0529-	•9177~ •9710~	•0194 •0185	•1598 •0438	•5577 •4190
100	77	463	60.00	15.00-	105.50	60.15	13-08-	2.6486	-6498-	•9907-	.0195	•0072-	-3385
100	78	464	70.00	15.00-	16.13	69.53	14.09-	2.9538	.0495-	•9915-	.0233	+0854	.4344
100	78	465	70.00	15.00-	21.50	69.58	14.09-	2.8106	•0501-	1.0313-	.0220	•1309	-5071
100	78	466	70.00	15.00-	32.25	69.66	14.10-	2.6380	•0460-	1.0942-	•0227	•1439	•5497
100	78 78	467 468	70.00 70.00	15.00~	43.00 64.50	69.77	14.11-	2.6558	.0439-	1.1616-	•0228	•0552	•4499
100	78	469	70.00	15.00-	107.50	70.44	14.13-	2.7618	•0506- •0630-	1-1802- 1-2365-	.0226 .0230	•0027 •0258-	•3837 •3433
100	79	470	80.00	15.00-	16.22	79.84	14.77-	د 960ء	.6273-	1.2168-	•0217	•0114-	.3082
100	79	471	80.00	15.00-	21.62	79.89	14.78-	2.8343	-0159-	1.2171-	.0168	+0054-	.3104
100	79	472	80.00	15.00-	32.43	79.99	14.78-	2.7412	.0229-	1.2245-	.0198	.0000	3423
100	79	473	80.00	15.00-	43.24	80.08	14.78-	2.6533	-6085-	1.4147-	•0124	+04C8-	+3017
100 100	79 79	474 475	80.00 80.00	15.00- 15.00-	108.10	80.3C 80.72	14.79-	2.6548	.0192- .0310-	1.4810-	.0126 .0153	•0632- •0768-	•3124 •3194
i	- 1												l
100 100	80	476 477	90.00 90.00	15.00- 15.00-	16.28 21.70	90.22	15.00-	2.9087 2.7364	.0049~ .0057~	1.7219-	.0083 .0079	•0067- •0125-	•3531
100	80	478	90.00	15.00-	32.55	90.32	15.00-	2.6712	.0112-	1.6140-	0085	0510-	.3592 .3544
100	80	479	90.00	15.00-	43.40	90.43	15.00-	2.6810	.0203-	1.6722-	.0085	·C578-	.3317
100	80	480	90.00	15.00-	65.10	90.66	15.00-	2.7285	.0321-	1.7422-	.0091	•C830-	.3322
100	aυ	481	90.00	15.00-	108.50	91.09	15.00-	2.7177	.0383-	1.8024-	.0085	•0959-	•3301
100	81	482	30.00	5.00-	15.16	30.03	2.51-	2.3427	-0174-	.7475-	.0012-	•0236	-0428
100	81	483 484	30.00 30.00	5.00- 5.00-	20.21 30.32	30.08	2.51- 2.52-	2.4039	-0181-	-8129-	-0008-	•0264	•0417
100	81	485	30.60	5.00-	40.42	30.23	2.52-	2.2432	•0139- •0116-	.8313- -8336-	.0001	•0102 •0072	.0234
100	81	486	30.00	5.00-	60.64	30.40	2.53-	2.2033	0109-	8344-	.0004	.0111	0086
100	81	487	30.00	5.00-	101.06	30.75	2.56-	2.2681	-0138-	.8407-	-0018-	-0155	.0245
106	82	488	40.00	5.00-	15.34	40.07	3.22-	3.1040	.0500-	.8043-	.0040-	.0190	.1031-
100	82	489	40.00	5.60-	20.45	40.12	3.23-	3.0071	.0449-	-8686-	.0103	.0039	.0691-
100	82	490	40.00	5.00-	30.68	40.22		2.8806	.0429-	•9478-		-0105	.0128
100	82	491	40.00	5.00-	40.90 61.35	40.52	3.24-	2.7023	.0381- .0411-	.9676- 1.0584-	.0276 .0252	.0026- .0004	.0208
100	82	493	40.00	5.00-	102.25	40.90	3.28-	2.6808	0288-	9915-	.0060-	.0217	.0067 .0301
100	83	494	50.00	5.00-	15.57	50.06	3.84-	2.8758	.0195-	.7223-	.0018-	•0258~	.0548-
100	83	495	50.00	5.00-	20.76	50.12	3.84-	2.9530	-0406-	6759-	.0256	•0049	-0355
100	83	496	50.00	5.00-	31.15			2.7689	-0382-	.8722-	-0051-	-0587	-1839
100	83	497	50.00	5-60-	41.53 62.29	50.31	3.85-	2.7520	-0381-	9415-	-0001-	•1055	•2023
100	83	499	50.00	5.00-	103.82	50.90	3.86-	2.6848	•0336- •0319-	9892-	.0038-	.0833 .0363	•1683 •1060
			<u>_</u>									1	

 $^{^{\}dagger}\text{Minus signs}$ are to the right of the numbers to which they apply.

TABLE III. - AERODYNAMIC COEFFICIENTS OF MODEL FOR THE COMPLETE INVESTIGATION - Continued

100 84 500		deg	lb/sq ft	deg	deg	CN	C _A	C _m	C _l	C _n	CY
1	60.00	5.60-	15.83	60.67	4.33-	2.8512	•5517-	•6951-		•2131	•394∠
100 84 501 100 84 502	60.00	5.00-	21.10	60.13	4.34-	2.9441	.0614-	•8547-		•2176	+4555
100 84 503	60.00	5.00-	31.65 42.20	60.23	4.34~	2.8083	-0579-	-9048- -د981		•1746	•3611
100 84 504	60.00	5.00-	63.30	60.54	4.34-	2.7595	6572-	1.0319-		•1309 •C175	•2958 •1311
100 84 505	60.00	5.00-	105.50	60.99	4.37-	2.8064	• Úp 90-	1.0508-		-6394-	•6491
100 85 506	70.00	5.00-	16.13	70.11	4.70-	3.6066	.0584-	∎9627 -	.0122	•1264	.2653
100 85 507	70.00	5.00-	21.50	70.16	4.70-	2.9351	.0566-	1.0345-	.0141	1748	.3483
100 85 508	70.00	5.00-	32.25	70.27	4.71-	2.8156	•049∠-	1.0935-	•0115	•1475	•2985
100 85 509 100 85 510	70.60 70.60	5.00-	43.00	70.38	4.71-	2.8278	.0473-	1.1726-	•0122	•0858	د218ء
100 85 510 100 85 511	70.00	5.00-	64.50 107.50	70.60 71.66	4 • 71 - 4 • 73 -	2.8151	•0552-	1.2083- 1.2578-	•0111 •0100	•0394 •0164	•1475 •1198
100 86 512	80.00	5.00-	16.22	80.15	4.92-	3.0592					
100 86 513	80.00	5.00-	21.62	80.20	4.92-	2.8704	•6383- •6388-	1.1596-		•0058- •0063-	•6973 •6827
100 86 514	80.00	5.00-	32.43	80.32	4.93-	2.9144	.0429-	1.2712-	.0106	•U126-	-0884
100 86 515	80.00	5.00-	43.24	80.42	4.93-	2.8145	-0386-	1.2714-	.0102	•0175-	•0913
100 86 516 100 86 517	80.00	5.00-	64 - 86	80.56	4+93-	2.8950	-0470-	1.3847-	•0105	•0215-	•0947
100 86 517	80.00	5.00-	108-10	81.11	4.94-	2.8644	.6554-	1.4277-	•3084	•0193-	•1008
100 176 1051 100 176 1052	60.00	• 60	15.83	60.18	•00	3.0775	-0589-	.7584-	•3035	•1274	+1554
	60.00	•60	21.10	60.22	•60	2 - 8456	0559-	-7587-	•0054	•1183	•1938
	60.00	•00 •00	31.65 42.20	60.33 60.44	•00	2.8107	.0530-	•9273- 1•0273-	•0032 •0027	•1241 •0647	•1755 •0895
100 176 1055	60.00	-00	63.30	60.66	•00	2.8046	.6584-	1.0720-	•00Z1	•0408	0093
100 177 1057	70.00		16.13	70.18	•00	3.0738	06.34	04.24	00.13		
100 177 1058	70.00		21.50	70.24	.00	2.9591	•0426- •0463-	.9626- 1.0007-	•0021 •0017	•0674 •1244	•0854 •1570
100 177 1059	70.00		32.25	70.35	•00	2.8902	.0463-	1.0966-	.0027	1336	•1776
100 177 1060	70.00	•00	43.00	70.46	•UG	2.9080	-0470-	1.1934-	0030	•0781	•0967
100 177 1061 100 177 1062	70.00 70.00	. LU	64.50 107.50	70.69 71.15	•U0	2.8800 2.8883	-0501- -0541-	1.2374-	•0013	•0440	•0551
1 1 1 1	ļ		- 1				•0541-	1.2790-	.0013	•0164	•0265
100 178 1063 100 178 1064	80.00	•00	16.22 21.62	80.∠0 80.∠4	•00	3.1020 3.0466	•0286- •0272-	1.1955-	•00ra	•0001- •0042-	-0110-
	80.CU	•00	32.43	80.36	.00	2.9563	.0332-	1.3127-	•0018	.0008	•0240- •0127-
	80.00	•00	43.24	80.46	.00	2.8575	.0364-	1.3039-	.0013	.0115	.0167
	80.06	•00	64.86	80.70	•00	2.8924	.0464-	1.3730-	•0013	•0098	.0164
100 178 1068	80.00	•66	108.10	81.16	••0	2.8819	•Ü523-	1.4366-	•0007	•0211	عادن. اعادن
	60.00	5.00	15.83	60.08	4.33	3.0021	.0497-	-6386-	•0017-		-1569
	60.00	5.00 5.00	*21.10 31.65	60.13 60.21	4.34	2.9489 2.6967	.0531- .0468-	•7635- •8686-	•0028- •0062-	•0500 •0713-	•0212-
	60.00	5.00	42.20	ز 60.3	4.34	2.7757	.0516-	1.0025-	.0062-	•0713~	•2035- •0881-
100 179 1673	60.00	5.00	63.30	60.54	4.35	2.7292	.0549-	1.0303-	•0059-	•0153-	.0989~
100 179 1074	66.00	5.00	105.50	60.98	4.37	2.7725	•0597-	1.0355-	.0043-	•0036	-0718-
	70.00	5.00	16.13	70.11	4.70	2.9920	.0339-	-9165-	.0064-	•0680	.0114
	70.00	5.00	21.50	70.16	4.70	2.9208	.0432-	.9387-	•00>6-	•0376	-0300-
	70.00 70.00	5.00	32.25	76.26	4.70	2.7820	-0388-	1.0887-	•0103-	•1093-	•2185-
	70.00	5.00 5.00	43.00 64.50	70.38 70.60	4•71 4•71	2.8356 2.8290	.0461- .0448-	1.1231-	.0068- .0091-	•0590 •0735-	•0015- •1637-
	70.00	5.00	107.50	71.06	4.73	2.8603	.0544-	1.2747-	.0084-		•108U-
100 181 1081	80.00	5.00	16.22	80.15	4.92	2.9385	.0215-	1.1037-	•0064-	•0090-	.0858-
	80.00	5.CU	21.62	80.20	4.92	2.8775	.0302-	1.1373-	.0067-	•0176	•0455-
	80.00	5.00	32.43	80.30	4.93	2.7580	•029∠-	1.2077-	-0065-	.0041	· 0735-
	80.00 80.00	5.00	43.24	80.43	4.93	2 • 8853	•0359-	1.3235-	.0075-	0129	-0791-
	80.00	5.00	108.10	80.64	4.93	2.8122 2.7840	•0434- •0526-	1.3370-	.0071- .0054-	•0159 •0367	•0741- •0430-
100 182 1087	60.00	10.60-	15.83	59.78	ا بيو						
	60.00	10.00-	21.10	59.84	8•66- 8•67-	2.7334	+0441- +0536-	•7525+ •8171-	.0169 .0157	•1813 •1832	•4946 •5344
100 182 1089 6	60.0U	10.00-	31.65	59.94	8.67-	2.7809	.0517-	8650-	.0138	•1632	•3479
	60.00	10.66-	42.20	60.04	8 • 68 -	2.7091	.0545-	9386-	.016d	•0426	.3093
	60.00	10.66-	63+30	60.24	8 • 70-	2.6935	.0577-	.9838- 1.0074-		•0167-	.2225
1	60.00	10.60-	105.50	60.67	8•74-	2.7202	•0597-	1.0074-	•0128	•0339-	•1759
	70.00 70.00	10.60-	16.13	69.89	9.40-	2.9077	.0552-	•9279-		•0931	•4113
	70.00	10.00-	21.50	70.05	9:40- 9:41-	2.8236	•0548- •0484-	.9884- 1.J426-		•1248 •0043	•4755 •2622
100 183 1096	70.00	10.00-	43.00		9.41-	2.7405	.0491-	1.0820-	•∪168	•6237-	.2022
100 183 1697 7	70.00		64.50	70.36	9.43-	2.7413	•S564-	1.1807-	.0179	•0163-	+2254
100 183 1098	70.00	10.00-	107.50	70.63	9.45-	2.7941	.0664-	1.2237-	.0182	•0021	•2443
	80.00		16.22		9-85-		•U379-	1.0968~	.0153	.0110-	•2739
	80.00 80.00	10.00-	21.62 32.43		9.85-	2.8252	.0437-	1.1001-	•0165	•0019	•2492
	80.00		43.24	80.40	9•85- 9•86-	2.7813	.0412-	1.2414-	0154	-0398- -0488-	•2310 •2194
100 184 1103 8	80.00	10.60-	64.86	80.52	9.86-	2.7904	.050B-	1.2684- 1.3238-	0173	•0488- •0598-	•2194 •2175
	80.00	10.00-		80.97	9 • 86 - 9 • 88 -	2.7816	.0574-	1.3741-	.0154	•0468-	•2156
		j	- 1	ł	l				-		

 $^{^{\}dagger}$ Minus signs are to the right of the numbers to which they apply.

TABLE III. - AERODYNAMIC COEFFICIENTS OF MODEL FOR THE COMPLETE INVESTIGATION - Continued †

			٦.		q,	α,	β,	Ι.	Τ		Γ_		
Config.	Run	Point	deg	ø, deg	lb/sq ft	deg	deg	C _N	CA	C _m	C1	Cn	CY
100	185	1105	60.00	15.00	15.83	59.30	12.97	2.9501	.0354-		.0213-	-1074-	•48≤6-
100	185	1106	60.00 60.00	15.00 15.00	21.10 31.65	59.34 59.43	12.98 12.99	2.7669	.0308- .0422-	•8366- •8833-	.0189-	•1574- •1799-	•5741- •6129-
100	185	1108	60.00	15.00	42.20	59.54	13.00	2.6372	.0472-	•907u-	.0180-	-0936-	•4791-
100	185	1109	60.00	15.00	63.30	59.74	13.03	2.6296	.0495-	1.0081-	.0187-	+1085-	4949-
100	185	1110	60.00	15.00	105.50	60.14	13.08	2.6336	-0540-	1.0315-	.0181-	•0345-	•3691-
100 100	186 186	1111 1112	70.00 70.00	15.00 15.00	16.13 21.50	69.51 69.58	14.09 14.09	2.8092 2.9176	.0436- .0928-	•9240- •9692-	.0266- .0232-	•0555- •0575-	.4836- .4186-
100	187	1117	80.00	15.00	16.22	79.82	14.77	2.7730	-0244-			•0257	•3419-
100 100	187 187	1118	80,00 80.00	15.00 15.00	21.62 32.43	79.88 79.98	14.78 14.78	2.7338	.0234- .0403-	1.1509-	.0168- .0170-	•0188 •0297	•3464- •3534-
100	187	1120	80.00	15.00	43.24	80.09	14.79	2.7230	0238-	1.4013-	0164-	•0358	-3477-
100	187	1121	80.00	15.00	64.86	80.29	14.79	2.6417	.0242-	1.4790-		•0364	-3208-
100	187	1122	80.00	15.60	108-10	80.74	14.81	2.7030	•0439-	1.5119-		•0885	+2546-
100	188	1123	60.00	20.00	15.83	58.58	17.25	2.6076	-0499-	•7935-		•1975-	•6761-
100	188	1124	60.00	20.00	21.10		17.26	2.6531	-0323-	-8657-		•1891-	•7009-
100	188	1125	60.00	20.00	31.65 42.20	58.72 58.81	17.28 17.30	2.5703	.0381- .0387-	•9838- •9487-		•2536- •1890-	.8178- .7141-
100	188	1127	60.00	20.00	63.30	59.00	17.33	2.4959	-0447-	.9760-		•0684-	5487-
100	186	1128	60.00	20.00	105.50	59.59	17.39	2.5359	-0465-	1.0606-	.0219-	.0175-	-4693-
100	189	1129	70.00	20.00	16.13	68.98	18.77	2.6949	+0582-	•7637-	•0231-	•0234	•4011-
100	189	1130	70.00	20.00	21.50	69.03	18.77	2.6559	•0438-	.8611-	•0234-	-0040-	•5012-
100 100	189	1131	70.00	20.00	32+25	69+13	18.78	2.5465	•0388- •0390-	1.0516-	•0238- •0241-	•0953-	•6291-
100	189	1132	70.00	20.00	43.00 64.50	69.21 69.43	18.79 18.82	2.5742	-0518-	1.0201-	•0241- •0259-	.0200- .1148	+5430- +3909-
100	189	1134	70.00	20.00	107.50	69.84	18.87	2.5872	-0700-	1.1283-		•1094	-3969-
100	190	1135	80.00	20.00	16.22	79.54	19.69	2.6123	.0058	1.2955-	•0192-	•0202	.3943-
100	190	1136	80.00	20.00	21.62	79.59	19.70	2.6141	•0101	1.2994-		.0276	-4230-
100	190	1137	80.00	20.00	32.43	79.67	19.70	2-5146	-0017-	1.3582-		•0119-	-4744-
100	190	1138 1139	80.00 80.00	20.00	43.24 64.86	79.78	19•71 19•72	2-5443	.0075- .0175-	1.4172-	•0190- •0197-	•0024 •0309	+4844- +4565-
100	190	1140	80.00	20.66	108.10	80.41	19.74	2.5886	0328-	1.4947-	-0198-	•0833	•3795-
100 100	285 285	1526 1527	80.00 80.00	15.00- 15.00-	16.22 108.10	79.82 80.73	14.77-	2.7170 2.6863	•0197- •0332-	1.1057-	.0179 .0132	•0459- •0590-	•3650 •3626
100 100	286 286	1528	80.00	15.00	16.22	79.84	14.77	2.9346	+0069-	1.2760-	•0147-	•0345	•3565-
		1529	80.00	15.00	108.10	80.75	14.81	2.7489	•0308-	1.4922-	•0163-	•0878	•2695-
100	287 287	1530 1531	80.00	15.00- 15.00-	16.22 21.62	79.84 79.88	14.77-		•0097- •0306-			•0320-	•3815
100	287	1532	80.00	15.00-	32.43	79.99		2.7212		1.1404-	•0205 •0192	•0447- •1827-	•3528 •2023
100	287	1533	80.00	15.60-	43.24	80.08	14.78-	2.6568		1.3389-	.0169	•1331-	•2200
100	287	1534	80.00	15.00-	64.86	80.49	14.79-	2.6304	-0180-		•0131	•0988-	•2779
100	287	1535	80.00	15.00-	108.10	80.72	14.81-	2.6679	•0411~	1.4755-	•0152	+0831-	•3157
100	288 288	1534 1535	70.00 70.00	15.00- 15.00-	16-13	69.51	14.09-	2.8070	0520-	-8279-	•0197	•0217-	•3297
100	288	1536	70.00	15.60-	21.50 32.25	69.57 69.68	14.09- 14.10-	2.7797 2.7594	•0457- •0415-	•9218- 1•0544-	•0228 •0075	•0121- •0825-	•3713 •2496
100	288	1537	70.00	15.00-	43.00	69.77	14.11-	2.6653	-0487-	1.0962-		•0713-	-2825
100	288	1538	70.00	15.60-	64.50	70.00	14-13-	2.7191	•0606-	1.2193-	•0204	.0106-	+3751
100	288	1539	70.00	15.63-	107.50	70.43	14-17-	2.7413	•U716-	1.2174-	•0229	•0308~	•3560
100	294	1545	70.00	15.00	16+13		14-09	2.9123	-د33-	•9500~	•0219-	•0262	•3653-
100 100	314 314	1617 1618	2.00	.∪ .∪	100.00	.∪ü 2.04	•00	.0127 .1394	-0444	.0005-	.0004	-0018-	-0052
100	314	1619	4.00	•00	100.00	4.09	•00	.2790	.0420 .0377	•0226- •0520-	.0004	.0004-	.0044
100	314	1620	6.00		100.00	6.15	•00	.4292	•0336	•U9QU-	.0004	.0010-	.0063
100 100		1621	8.00 10.00	.00	100.00 100.00	8.20 10.26	•00	•5795 •7401	•0301 •0271	•1353- •1942-	.0002 .0001	.0013- .0011-	•0075 •0059
102	315	1623	.QU		100.00	.02-	.00	.0433-	.0474	.0841	.0063	•C018-	•C058
102	315	1624	2.00	. ↓0	100.00	2.63	.00	.0860	-0446	•0585	.0004	.001C-	•0056
102 102	315 315	1625 1626	4.00 . 6.00	•66 •66	100.00	4.67 6.13	•00 •00	.2253 .3697	•0396 •0344	.0289 .0008-	•0006	•0009-	•0069
102	315	1627	8.00	•00	100.00	8.18	•00	.5191	•0344 •0305	•0008- •0399-	.0005 .0007	.0010-	•0066 •0069
102	315	1628	10.00	•00	100.00	10.24	.00	.6668	.0264	.0895-	.0004	.0011-	د ځان ه

 $^{^{\}dagger}\text{Minus signs}$ are to the right of the numbers to which they apply.

TABLE III. - AERODYNAMIC COEFFICIENTS OF MODEL FOR THE COMPLETE INVESTIGATION - Continued

Config.	Run	Point	α ₁ , deg	ø, deg	q, lb/sqft	α, deg	β, deg	C _N	C _A	C _m	c _l	C _n	С¥
104	316	1629	•00	• 60	100.00	. 05-	.00	.1274-	.057.7	.2024	.0015-	•0039-	+0068
104	316	1630	2.00	* U	100.00	2.00	. ∪ Q	.0069	• 6535	•1644	*0016-	-0027-	•0055
104	316	1631	4.00	• 6 9	100.00	4.05	.00	•1490	.0480	•1405	.0016-	•0018~	•0036
164	316	1632	6.0C	<u>. ي</u> ن	100.00	6.10	.00	2986	.419	•0996	.0013-	•0018-	•0055
104	316 316	1633 1634	.8.00 10.00		100.00	8.15	.00 .00	.5951	•0368 •0323	+0612 +0145	*0010-	•0013- •0015-	•0042 •0037
106	191	1141	.uu		15.00	• i. 2-	.00	.3728-	.2203	<u>.</u> 5428	.0017	•0021-	.0118
106	191	1142	ÜÜ		20.00	. ŭ 3 -	.00	3995-	.2196	•5588	.0026	.0018-	.0149
106	191	1143	.0u	•60	30.00	.04-	• U Û	.3666-	•∡184	.5362	-0019	.0023-	+0142
156	191	1144	_ UL		40.00	• ∨5-	•∪0	.3642-	.2118	•5256	.0026	+0041-	+0144
106	191	1145	ا بان	• 66	60.00	•∪8-	•00	.3522-	•2084	.5144	•00∠7	-0030-	•0089
106	191	1146	•00	٠٠٠	100.00	•13-	•00	.3382-	.2079	+5025	3 د ۵۵۰	•0026~	•0091
196	192	1147	5.00	ن ي و	15.00	4.99	•00	.1321-	•2161	•5841 •5674	.0009	•0117- •6073-	•0503 •0336
106	192 192	1148	5.00 5.00	. UU . UU	20.00 30.00	4.99 4.99	•00	.1172- .1002-	.2136 .2050	•5334	.0014	•0049-	-0241
106 106	192	1150	5.00	.00	40.00	4.99	.00	.0868-	1938	•5075	.0018	•0027-	.0119
106	192	1151	5.00	.00	60.00	4.97		.0736-	.2017	5196	.0020	.0025-	-0119
166	192	1152	5.00	100	100.00	4.97	.00	-0565-	•1987	.5085	.0027	-0016-	+0087
1.06	193	1153	10.60	•60	15.00	10.61	•00	.2295	د د 183 ه	•4904	.0002	-0084-	.0331
106	193	1154	16.00		20.00	16.01	•∪¢	.2447	-1816	.4707	•0009	•0048-	•0193
106	193	1155	10.00	• (U	30.00	10.02	•06	.2339	•1836	4819	.0012	+0016-	•0090
106	193	1156	19.00	•00	40.00	10.02	•00	.2348	+1838	•4846	.0011	-0015-	•0080
106 106	193 193	1157 1158	16.00 10.00	.ΩU .UU	60.06 100.00	10.04 10.08	.00	.2432	•1847 •1835	.4863 .4788	.0013	+0014- +0009-	•0066 •0046
106	194	1159	15.00	•60	15.00	15.03	•00	.5723	.1806	• 4745	.0005-	.0013-	,0089
106	194	1160	15.00	ين.	20.00	15.03	.50	.5541	•1696	4074	.0008	-0006-	0038
106	194	1161	15.00	.00	30.00	15.04	••0	4926	.1693	4261	.0002	•0010	.0020-
136	194	1162	15.00	20	40.00	15.08	.00	5063	•1721	4379	.0003-	.0002-	+0010
106	194	1163	15.00		60.00	15.11	•00	.5153	•1707	.4286	.0004-	•0005-	+0034
156	194	1164	15.0-	.00	100.00	15.19	•UC	•5246	•1714	•4335	.0008-	•0007-	+0011
106	195	1165	20.00	•CU	15.00	20.05	•00	•9210	.1346	2990	.0021-	-0067	-0209-
106	195	1166	20.00	•00	20.00	20.07	•UC	.8819	•1242	-2531	•0013-	-0064	•0192-
106	195	1167	20.00 20.00	•00	30.00 40.00	20.10 20.12	•00	.8603 .8284	•1274 •1234	•2678 •2646	.0024- .0018-	+0066 +0047	.0132-
106 106	195 195	1168	20.00	 	60.00	20.12 20.19	•00	8641	1252	.2617	•0020-	•0027	.0061-
106	195	1170	20.00	.00	100.00	20.33	.00	.8848	.1237	.2625	.0021-	.0017	.0058-
106	196	1171	36.00	.:0	15.16	30.10	•40	1.8400	.0172	.0149-	.0071	.0006	-0600-
106	196	1172	30.00		20.21	30.13	•00	1.7276	.0156	.0733-	.0041	•0050-	.0277
166		1173	30.00	•00	36.32	30.18	•00	1.5824	.0117	-1046-	•0027~	•0025	+0061
106	196	1174	30.00	•00	40.42	30.23	•00	1.5420	•0077	•1305-	.0033-	•0008	+0089-
106 106	196 196	1175 1176	30.00 30.00	•@∪ •00	101.06	30.36 30.62	•00	1.5841	.0078 .0058	•1395- •1392-	.0009-	+0016 +0038~	.0027-
106	,,,,	1177	40.00	•00	15.34	40.14	•00	2.5065	.0750-	.0907-	.0005	.0031-	.0868
106	197 197	1178	40.00	•60	20.45	40.14	.00	2.4446	.0920-	.1706-	.0014	.0011	.0497
106	197	1179	40.00	.00	30.68	40.24	•00	2.1462	0750-	.2701-	.0063-	.0083	.0318
106		1180	40.00		40.90	40.33	•00	2.1652	-8080-	-3601-	.0036-	-0147	0095
106	197	1181	40.00	•00	61.35	40.49	•00	2.1409	.0829~	•3866 -	.0027-	-0042	-0060-
106	197	1182	46.60	•63	102.25	40.80	-00	2.1233	•0827-	•3733-	•0017	•0562-	•0393-
106	198	1183	50.00	.00	15.57	50.14	•00	2-4009	.0865~ .1098-	.2883- .2692-	.0204- .0002-	•1214- •0671-	•2504- •2223-
106	198	11.84 1185	50.00 50.00	•60	20.76 31.15	50.19 50.27	•00	2.5300	.1150-	.4222-	.0002-	•0257~	.0361-
106	198 198	1186	50.00	00. Ju	41.53	50.37	•00	2.4044	1196-	4968-	.0010	-1101-	•1511-
106		1187	50.00		62.29	50.52	.00	2.2733	.1209-	5208-	.0000	.0652-	.0882-
106	198	1188	50.00		103.82	50.87	•00	2.2715	.1252-	.5224-	.0018-	•0859-	+1287-
106	199	1189	60.00	•00	15.83	60.16	•00	2.7886	.1535-	•3587-	•0009-	-1930-	-2807-
106	199	1190	60.00	• 60	21.10	60.20	•00	2.6178	.1486-	.4544-	.0621	•1771-	-2694-
1.6		1191	60.00	•60	31.65	60.30	•00	2.5233	•1535-	•5312-	.0007-	-2503-	.3169-
106	199		60.00	•00		60.39	•00	2.4854	•1618-	•6221-	.0027-	0740	.2698- .1089-
106 106	139	1193	60.00 60.00	•60	63.30 105.50	60.97	•00	2.4790 2.4766	•1758- •1795-	.6968-	.0027- .0015- .0007	•0091-	·1089-
106	200	1195	70.00	•60	16.13	70.17	.00	2.8419	.1775-	.7848-	.00uB	.0429-	.0834-
	200		70.00		21.50	70.21	•00	2.6541	.1609-	•6545-	.0004	.0531-	-1108-
106	200	1197	70.00	•00	32.25	70.30	•00	2.5446	.1594-	•7275-	.0018	+0814-	1109-
106	200	1198	70.00	. Cü	43.00	70.39	-00	2.4499	-1588-	.76∠∠-	-0018- -0100-	0305	.0212
106	230 200	1199 1200	70.00 70.60	•00 •00	64.50 107.50		•00	2.5174	•1737- •1830-	.8673- .8511-	.0010-	•0582 •0706	.0513 .0546
ļ		ì	1		Į.	l .		2.7819		0044	0001	.0108	.0400-
106 106	201		80.00	•60 •60	21.42	80.17 80.∠1	•00	2.6792	.1362-	8836-	-0005		.0416-
	201 201	1203	84.00	.00	32-43	80.32	.00	2.6326	1480-	9764-	.0005	.0023	0249-
	201		80.00	•00	32.43 43.24	80.41	.00	2.5494	.1541-	.9046- .8836- .9762- 1.0053- 1.0276- 1.1562-	.0003	-0143	-0116-
		1			1 / 2	80.60	.00	2.4881	1629-	1 - 0276-	-0005	.0194	.0043
	201 201	1205	80.00 80.00	ن⊋∙	108.10		.00	2.5834		1.002.10		0271	0151

 $^{{}^{\}dagger}\text{Minus signs}$ are to the right of the numbers to which they apply.

TABLE III. - AERODYNAMIC COEFFICIENTS OF MODEL FOR THE COMPLETE INVESTIGATION - Continued

Config.	Run	Point	α ₁ , deg	g, deg	lb/sq ft	æ, deg	β, deg	CN	C _A	C _m	c ₁	C _n	C Y
166	202	1207	90.00	•ců	16.28	90.18	•60	2.9868	1914-	1.4061-	•0003-	•0041	-0165-
106	202	1208	90.00	•60	21.70	90.22	•00	2.7364	-1815-	1.2846-	-0007-	•0067	-0261-
106 106	202	1209 1210	90.00 96.00	.00	32.55 43.40	90.33	•00	2.7504	•1995- •1933-	1.3542-	.0007-	.0018- .0058	.0133- .0075-
106	202	1211	90.00		65.10	90.61	.00	2.5410	-4086-	1.3424-	.0003-	0102	.0026
166	252	1212	94.00		108.50	91.63	•00	2.5637	•2169-	1.3993-	.0005-	.0320	•0269
167 167	203 203	1213	.00		15.00	.02	•00 •00	.3393	.3889 .0910	.4310- .4078-	.0013	.0136	.0317- .0100-
167	203	1214	00		30.00	.02	•00	2945	.0888	.3956-	•0010	.0035	.0010
167	263	1216	GU		40.00	.05	.00	.3071	.0923	.4075-		,0040	-0042-
107	203	1217	.00		60.00	•67	•00	.3062	.0916	.4057-	.0006	.0027	-0023-
157	203	1218	-00	•0-	100.00	-11	•00	.2900	•⊍917	•3929-	•0005	•0009	•0035
107	204	1219	5.00	•00	15.00		•00	•6508	•0904	.4725-	.0009	•0103	-0096-
107	204	122C	5.00	-60	20.00	5.04	•00	•6453	.0889	•4723-	-0007	•0091	-0106-
167 167	204	1221	5.00		40.00	5.06 5.08	•00 •00	•6486 •6300	•0941 •0909	•4784- •4662-	.0005	.0060 .0048	+0061- +0051-
107	204	1223	5.00	1	60.00	5.13	•00	.6293	•3895	.4652-	.0006	-0028	-0030-
157	204	1224	5.00		100.00	5.24	•00	.6393	. 3917	.4683-	.0005	+0012	•0002
157	265	1225	16.60	۰۵۰	15.00	10.05	•60	1.0132	•∂953	•5829-		.0151	-0253-
107	205	1226 1227	10.00 10.00		20.00 30.00	10.07	•00	1.0596	•3922 •3959	.6023- .5815-		.0130 .0089	-0239-
157	205	1228	16.60		40.00	10.14	•00	9858	1922	.5635-		-0064	.0123-
157	205	1229	10.00		60.00	10.22	•00	1.0132	.3941	.5789-		0026	.0036-
157	265	1230	10.00		100.00	10.36	•00	1.0069	•0959	•5734-	.0005	.0011	.0004
107	206	1231	15.60	.00	15.00		•00	2.2457	.0913	1.1864-	.0005	-0196	.0311-
107	206	1232	15.00	•60	20.00		•00	1.3572	•0987	•6974-	.0009	.0147	•0278-
157	206	1233	15.00	د د د	30.00	15.14	•00	1.3653	-1041	.7068-	.0001	-0087	+0149-
167 157	206	1234 1235	15.00 . 15.00	•00	60.00	15.19 15.29	•U0	1.3309	•1012 •1023	.6880- .6931-	.0002-	.0061 .0031	.0053- .0029-
157	206	1236	15-60		100.00	15.50	.00	1.3572	.1075	.6962-	.0010-	.0017	.0012-
1.7	207	1237	20.00		15.00	20.16		1.7737	003	.8397-		-0166	.0329-
167	207	1238	20.0L	٠٥٥	20.00	20.13	•00	1.7601	• .039	.8512-		.0176	-0380-
107 107	207 207	1239 1240	20.00	•00 •00	30.00 40.00	20.19	•00	1.6939	• 018 • 006	.8172- .8100-		•0119 •0105	.0237- .0165-
167	207	1241	20.00		60.00	20.38	.00	1.7053	021	-6163-		•0070	0095-
167	267	1242	20.00	.50	100.00	20.65	.00	1.7472	047	.8267-		•0050	-0029-
167	208	1243	30.00	ن ي .	>15+16	30.15	•00	2.6746	•0792	1.0130-	.0012	•0093	-0228-
107	208	1244	30.00		20.21	30.19	•00	2.4975	835	1.0217-	+0014	•0196	•0153-
107	208	1245	30.00	• 60	30.32 40.42	30.27 30.36	•00	2.3967	•□856 •□858	1.0437-	•0002	•0072	-0057-
107 107	208 208	1246	30.00 30.00	.00	60.64	30.55	•00	2.4386	878	1.0666-	.0007-	-0002 -0037	•0092- •0040
107	208	1248	36.CL	.00		30.92	.00	2.4713	.⊍870	1.0725-	.0004-	•0018	-0085
167	209	1249	40.00	• (16	15.34	40.19	•00	3.3244	• 1478	•9168-	.0345-	.0599	-3678-
107	209	1250	40.00	• CU	20.45	40.24	•00	3.1884	• 1523	-9852-		-0141	1945-
107 107	209	1251 1252	40.0L		30.68 40.90	40.34	•00 •00	2.9816 2.8471	• 1574 • 1579	1.1250-	.0083	+0018 +0069-	.0372-
107	209	1252	40.00	:00	61.35	40.64	•00	2.8184	580	1.1475-	.0039	-0122-	.0119- .0513-
107	269	1254	40.00	.25	102.25	41.03	•00	2.7126	• 1628	1.0877-	.0116	-0011	-0852-
107	210	1255	50.00		15.57	50.18	•00	3.0498	- 1594	.8413-	.0092-	-1412-	-2922-
107	210	1256	50.00	•00	20.76		•00	2.9594	• 457	.7954-	.0113	-0771-	-2451-
107	210	1257	50.00 50.00	•66	31.15 41.53	50.34	•00	2.9360 2.7359	• 477	-9833~	.0080 .0045	-1213-	+2022-
107 107	210	1258 1259	50.00	.00	62.29	50.64	•00	2.7584	• 479 • 488	1.0167-		+0647- +0486-	•1148- •0723-
107	210	1260	50.00		103.82	51.07	.00	2.7833	- 483	1.0882-	.0015-	.0677-	-0935-
107	211	1261	60.0u	•£0	15.83	60.18	•00	3.0995	- 301	.7872-		-1790-	-3101-
107	211	1262	60.00	.66	21.10	60.23	•00	2.9972	- 294	.8906-		•1813-	.3045-
107	211	1263	60.00	٠.		60.33		2.8560	237	-9314-		-2578-	-3571-
107 107	211	1264	60.00	. (, t	42.20 63.30	60.45	•00	2.8701 2.8871		1.0778-		•0649-	-1078- -0491-
167		1266	60.00		105.50		•00	2.8832	•1 181 •1 141	1.1567-	.0007	+0362- +0068	.0061
167	212	1267	70.00	•6u	16.13 21.50	70-18	•00	3.0665	• 167	.9290- 1.0098-	-0044	•0769	-0331
167	212 212 212	1266	70.00	•60		70.24	•00	3.0348	•! 213 • 263	1.0098-	.0011-	-0806-	-1285-
167 167	212	1269 1270	70.00 70.00		32.25 43.00	70.35 70.47	•00	2.9397 2.9340	1253	1.1390-	.0009-	.0482- .0781	.0765-
107	212	1271	70.00		64.50	70.70	•00	2.9256	1241	1.2692-	.0018	•0781 •0541	-0544
107		1272	70.00	٠٥٠	107.50	71.16	.00	2.9202	• 183	1.2809-	.0011	-0717	.0720
107		1273	8C.0J	•00	16.22	80.20	•00	3-1069	. (450	1.2231-	.0019	-0118	.0403-
107		1274	80.00	•60	21.62	80.24		3-0476	•1 366	1.2144-		-0011-	
107 107	213 213		80.00 80.00	•60 •60	32.43 43.24	80.48	•00	3.0763 2.9180	• 417 • 360	1.3733-	.0004	•0050-	
107	213		80.00	.00	64.86		-90	2.9180	. 306	1.4210-	.0004	-0121 -0084	.0002
107	213	1279	80.00	.00	108-10		900	2.7339	-(247	1.3616-	-0001-	-0141	.0174
	Ll	L		L									

 $^{^{\}dagger}$ Minus signs are to the right of the numbers to which they apply.

TABLE III. - AERODYNAMIC COEFFICIENTS OF MODEL FOR THE COMPLETE INVESTIGATION - Continued

Config.	Run	Point	α ₁ , deg	g, deg	q, lb/sq ft	α, deg	β, deg	c _N	C _A	C _m	c,	Cn	CY
107	214	1279	90.05	•00	16.28	90.17	• 20	2.8731	•1049	1.6357-		•0168	+0207-
107 107	214	1281	90.00	•00	21.70 32.55	90.23	•00	2.8730	•0977 •0938	1.6683-	.0000	•0123 •0031	-0422-
107	214	1282	90.00	00	43.40	90.45	-00	2.8232	0927	1.7422-	.0016-	.0070	.0310-
107	214	1283	90.00	:00	65.10	90.67	.00	2.7713	.0810	1.7751-	.0006-	0084	.0006
107	214	1284	90.00	.60	108.50	91.06	.00	2.6451	•075≥	1.7387-	.0010-		-0272
110	215	1285	•00	•00	15.00	.00	•00	•0198	.0425	.0020-	-0009-		-0365-
110	215	1286	•00	.00	20.00	.00	•00	•0145	•0448	•0067	.0007-	-0058	-0274-
110 110	215 215	1287 1288	•00 •00	•60	30.00 40.00	.00	•30	•0273	-0441	.0093-	.0005-	+0044	-0182-
110	215	1289	- QU	 	60.00	.00	.00	.0268 .0178	•0451 •0442	.0086-	.0001-	•0038 •0016	.0139-
110	215	1295	.03	.60	106.00	.01	.00	.0210	.0449	.0027-	.0000	.0014	•0045-
110	216	1291	5.00	•60	15.00	5.01	•00	.3634	.0365	.0723-	.0012-	•0095	.0443-
110	216	1292	5.00	•00	20.00	5.03	.00	•3756	•0376	•0855-	.0001-	-0089	•0351-
110	216	1293	5.00	•00	30.00	5.03	•00	•3796	•0371	•0886-	-0001-	•0067	-0259-
110 113	216	1294 1295	5.00 5.00	.;u .;ü	40.00	5.04	•00	.3621	-0377	•0742-	.0001-	+0061	.0221-
110	216	1296	5.00	.00	100.00	5.07 5.13	•00	.3708 .3696	.0373 .0364	.0771- .0770-		.0049 .0031	-0155- -0098-
110	217	1297	10.00	• 60	15.00	10.64	•00	.8287	.0272	.2348-	.0005-	.6239	-0916-
110	217	1298	10.06	•00	20.00	10.05	.00	.8281	-0277	-2408-	.0005-	.0202	-0792-
110	217	1299	10.00	ن ټ و	30.00	10.08	•00	.7944	•0285	•2229-	-0002-	.0130	-0520-
110	217	1300	10.00	• 60	40.00	10.11	•00	•7836	•0283	•2122 -	.0003-	•0118	-0437~
110 110	217 217	1301 1302	10.00	•00 •00	100.00	10.16 10.27	.00	.7676 .7601	•0282 •0189	•2068- •2022-	.0002 .0001	•0078 •0045	•0285- •0165-
110	218	1303	15.00	• 00	15.00	15.06	•00	1.2606	.0202	.4219-	.0003-	•0397	+1456-
110	218	1304	15.00	.00	20.00	15.09	•00	1.2302	.0233	4065-	.0001	.0321	1131-
110	218	1365	15.00	.00	30.00	15.12	•00	1.1589	.0221	.3871-		•0224	.0788-
110	218	1306	15.CU	•00	40.00	15.17	•00	1.1476	.0230	3697-		.0188	-0648-
110	218	1307	15.00	•00	60.00	15.26	•00	1.1622	•0223	.3715-	.0001-	-0126	-0408-
110	218	1308	15.00	•60	100.00	15.42	•00	1.1381	•0226	.3563-	-0012-	•0076	-0244-
110 110	219 219	1309 1310	20.00 20.00	•00 •00	15.00 20.00	20.09	.00	1.7082	.0113	-6042-		•0530	-2003-
110	219	1311	20.00		30.00	20.12	.00	1.6339	.0125 .0127	•5852- •5648-	.0001 .0002-	+0385	•1448- •0961-
110	219	1312	20.00		40.00	20.23	.00	1.5630	.0134	-5458-	.0002-	•0263 •0222	-0780-
110	219	1313	20.00		60.00	20.34	.00	1.5332	.0129	.5237-	.0004	.0149	-0506-
110	219	1314	20.00		100.00	20.57	•00	1.5525	.0128	-5178-	.0001-	.0078	-0290-
110	220	1315	30.00	•00	15.16	30.14	•00	2.5809	.0127-	•9347-	.0012	•0552	-2147-
110	220	1316	30.0u	•00	20.21	30.19	•00	2.4840	.0131-	•9049-	.0031	•0346	•1494-
110 110	220	1317 1318	30.00 30.00	• 00	30.32	30.27	•00	2.3840	-0114-	.8637-	.0014	+0263	-1034-
110	220	1319	30.00	•60 •60	40.42 60.64	30.35 30.52	•00	2.3655	-0119-	.8546- .8238-	-0008	•0178	•0712-
110	220	1320	30.00	0	101.06	30.87	.00	2.3250	.0115- .0225-	.7999-	•0005 •0021	.0139 .0024	•0534- •0219-
110	221	1321	40.00	ال ال	15.34	40.18	.00	3.2248	.0456-	•9791-	.0096	.0537	.2309-
		1322	40.00	• 60	20.45	40.24	.00	3.1705	•0431~	•9722-	.0124	.0403	-1848-
110	221	1323	40.00	• U	30.68	40.34	•00	2.9724	•0390-	•9522-	-0107	•0257	•1123-
110 110	221	1324 1325	40.00 40.00	•60	40.90	40.44	•00	2.9289	-0385-	•9597-	.0067	•0208	+0761-
110	221	1326	40.00	•00 •60	61.35 102.25	40.64 41.09	•00	2.8290	•0354- •0359-	•9279- •9231-	.0031- .0015-	•0142 •0121	-0413- -0313-
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110	222	1327	50.00	•00	15.57	50.19	•00	3.3417	.1661-	2.5560-	•0037	•0021	•0274-
110 110	223 223	1333 1334	60.00 60.00	•00	15.83 21.10	60.19 60.23	•00	3.1600 2.9893	•1260 •0808	•6789- •6592-	•0048 •0035	•0454 •0525	•1613- •1291-
		1339	70.00	•60	16.13	70.20	•00	3.2754	.1254	.9460-	.0012	•0555	-1781-
		1340	70.00	•00	21.50	70.25	•00	3.1909	0852	•9833-	•0024	.0617	-1147-
		1341	70.00	•00	32.25	70.35	•00	2.8923	0533	•9787-	•0028	•0428	.0701-
		1342 1343	70.00 70.00	• C U	43.00	70.45	•00	2.8569	.0383	1.0051-	•0013	•0251	•0589-
110		1344	70.00	.00	64.50 107.50	70.70 71.18	•00	2.9332 2.9690	.0179 .0025	1.0836-	.0012 .0011	.0158 .0093	•0398- •0236-
		1345	80.00	.00	16.22		.00	3.0967	•1383	1.1482-	.0023	•0456	.2030-
		1346	80.00	•00	21.62	80.24	•00	3.0452	0993	1.1386-	-0014	•0375	•1531-
		1347	80.00 80.00		32.43	80.36		2 9954	•0563 0317	1.2348-	.0009	•0247	•0862-
		1348	80.00	.00	43.24 64.86	80.48		3.0010 2.9614	•0317 •0116	1.2598-	.0015 .0006	.0193 .0108	.0618- .0433-
		1350	80.00	.00	108.10			2.8104	.0008-	1.2302-		-0005-	.0257-
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 $^{^{\}dagger}$ Minus signs are to the right of the numbers to which they apply.

TABLE III. - AERODYNAMIC COEFFICIENTS OF MODEL FOR THE COMPLETE INVESTIGATION - Continued

Config.	Run	Point	α ₁ , deg	ø, deg	q, lb/sq ft	α, deg	β, deg	c _N	CA	C _m	C ₁	Cn	CY
110	226	1351	90.00	ان،	16.28	90.19		3.1161	-1403	1.6648-		•0789	-1603-
110	226	1352	90.00	• 60	21.70	90.24	•00	2.9875	•1031	1.6209-		•0362	-1681-
110	226	1353 1354	90.00	03.	32.55	90.35	•00	2.8734	.0651 .0449	1.6033-	.0007	•0237 •0174	•1150- •0808-
110	226	1355	90.00	.00	65.10	90.69	.00	2.8611	.0226	1.6267-	.0002	.0136	.0486-
110	226	1356	90.00	.00	108.50	91.09	.00	2.7196	.6105	1.5799-	.0003-		.0289-
110	227	1357	30.00	5.00-	15-16	30.05	2.51-	2.4626	.0142-	.8363-	.0018	-0114	.0511-
110 110	227	1358 1359	30.00 30.00	5.00-	30.32	30.15	2.52-	2.2632	.0135~ .0143~	•7755- •7663-	.0042-	+0117 +0142	-0420- -0447-
110	228	1360	40.00	5.60-	15.34	40.07	3.22-	3.0925	.0438-	.8599-	.0299	.0040-	.0843-
110	229		50.00	5.00-	1			3.0498	1		1	ļ	
110	229	1363 1364	50.00	5.00-	15.57 31.15	50.21	3.84-	2.7766	•0262- •0427-	•6048- •6174-	.0053 .0145	•0517- •0426-	•0517- •0223
110	230	1366	60.00	5.00-	15.83	60.67	4.33-	2.9952	.0213-	.6711-	.0086	-0286-	.0870
110	230	1367	60.00	5.00-	31.65	60.24	4.34-	2.8761	.0331-		-0065	.0313-	.0663
110	230	1368	60.00	5.00-	105.50	61.04	4.38-	2.9335	.0360-			.0047-	-0966
110	231	1369	70.00	5.00-	16.13	70.11	4.70-	2.9588	.0294-	.8120-	.0085	.0018-	-1042
110	231	1375	70.00	5.00-	32.25	70.28	4.71-	2.9574	.0229-		-0098	.0064-	-0889
110	231	1371	70.00	5.00-	107.50		4.73-	2.8952	•0192-			•0157	•0599
110	234	1372	80.00	5.00-	16.22		4.92-	3.0362	-0162-	1.1034-	•0034	.0029	-1186
110	232	1373	86.00	5.00-	32.43	80.31	4.93-	2.8404	.0186-	1.1735-	.0089	.0048-	+1114
110	232	1374	80.00	5.00-	108-10	81.11	4.94-	2.8650	.0212-	1.2685-	.0080	•0093-	•1069
110	233	1375	90.00	5.00-	16.28	90.17	5.00-	2.9035	.0680-	1.5453-	-0044	-0418	•1709
110 110	233	1376 1377	90.00 90.00	5.00-	32.55 108.50	90.35	5.00- 5.00-	2.8853	.0115-	1.6218-	•0040 •0035	+0047-	•1242
1			1 .				i	2.0204	.0151-	1.0752-	•0033	•0203-	•1063
110	234	1378	10.00	10.00-	15.00	9.88	1.74-	• 7394	.0244	-1852-	•0034	.0061-	•0130
110 110	234	1379 1380	10.00 10.00	10.00-	30.00 100.00	9.92	1.74-	•7224 •7304	.0259	•1815- •1841-	.0029 .0028	•0097- •0144-	•0263 •0387
110	235	1381	20.00	10.00-	15.00	19.80	l	1.4542		1		ŀ	1 1
110	235	1382	20.00	10.00-	30.00	19.88	3.42-	1.4376	.0093 .0114	.4538- .4800-	.0010- .0013-	•0024- •0039-	•0089 •0231
110	235	1383	20.00		100.00	20.26	3.49-	1.5132	.0066	.6455-	.0044-	-0133-	-0535
110	236	1384	30.00	10.00-	15•16	29.75	5.00-	2.3418	.0134-	.7340-	.0003-	.0049	.0463-
110	236	1385	30.00	10.66-	30.32	29.88	5.02-	2.3147	.0126-	7579-	.0030-	•0107	-0812-
110	236	1386	30.0€	10.00-	101.06	30.45	5-10-	2.2528	.0132-	•7525-	.0103	.0222	•0717-
110	237	1387	40.00	10.00-	15.34	39.73	6.43-	3.1021	.0611~	.8634-	.0114	.0252-	-1051-
110	237	1388	46.00	10.00-	30.68	39.88	6 • 45-	2.8295	-0345-	.8138-	•0055	.0109~	-1962-
110	237	1389	40.0L	10.60-	102.25	40.58	6.54-	2.7381	.0302-	.7983-	•0311	•0563-	•0097-
110	238	1390	50.66	10.00-	15.57	49.73	7.66-	2.7784	.0234-	•4878-	.0041	•1379-	-0566-
110		1391 1392	50.00 50.00	10.00-	31.15 103.82	49.88 50.60		2.7517	0203-	•5648-	.0129	•1434-	•0092-
							I	l .	.0243-	+7144-	•0010	-0661-	-1001
110 110	23 / 239	1393	60.00 60.00	10.00-	15.83 31.65	59.79 59.95		2.9225	-0322- -0355-	•5547- •6105-	•0104	•1178-	•1217
110		1395	60.00		105.50	60.71		2.7939	.0358-	·8097-	.0126 .0142	•0900- •0214-	•1315 •1918
110	240	1395	70.00	10.00-	16.13	69.89	9.40-	2.8367	.0348-	.7818-	0367	0124-	24.00
iio	240	1396	76.00	10.00-	32.25	70.06	9.41-	2.8550	-2385-	•9666-	•0167 •0181	•0136- •0487-	•2480 •2018
110	240	1397	70.00	10.00-	107.50	76.83	9.45-	2.8059	.0251~	1.0757-	•0179	-0181-	•2244
110	241	1398	80.00	10.00-	16.22	80.04	9.85-	2.9607	-0174-	1.1295-	•0171	•0021	-2521
110		1399	80.00	10.00-	32.43	80.20	9.85-	2.8683	-0184-	1.1893-	•0156	•0198-	-2391
116	241	1400	80.00	10.00-	108.10	80.95	9.87-	2.7294	0223-	1.2195-	.0134	•0091-	+2192
1,10		1401	90.uu	10.00-	16.28			2.9454	-0095-	1.6304-		.0109	-3406
110	242	1402	90.00 90.00	10.00- 10.00-	32.55 108.50	90.53	10.00- 10.00-	2.7968 2.8547	0130- 0169-	1.6155-		-0104	-2880
				-				246541	0169-	1.7016-	.0072	-0376-	•2650
110		1405 1404	26.00 U	15.60-		19.53		1.4519	0147	•4726-	.0049-	+0155-	•0705
110		1404	20.00 20.00	15.00-	15.00	19.45	5.09- 5.20-	1.4963	0126 0141	•4713- •4777-	•0039- •0071-	•0126- •0150-	•0623 •0637
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110 110	244 244	1407 1408	30.00 30.00	15.00- 15.00-	15.16 30.32	29.27 29.40	7.46- 7.49-	2.2784	0016- 0036	•6750- •7585-	+0003- +0046	•0022- •0057-	•1058- •1182-
110		1409	30.00	15.00-	101.06	29.93	7.61-	2.2090	0038-	.7267-	.0108	.0182	•0944-
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 $^{^{\}dagger}$ Minus signs are to the right of the numbers to which they apply.

L-905

TABLE III. - AERODYNAMIC COEFFICIENTS OF MODEL FOR THE COMPLETE INVESTIGATION - Continued

Config.	Run	Point	α ₁ , deg	ø, deg	q, lb/sq ft	α, deg	β, deg	C _N	C _A	C _m	C,	C _n	CY
110 110 110	245 245 245	1410 1411 1412	40.00 40.00 40.00	15.00- 15.00- 15.00-	15.34 30.68 102.25	39.19 39.33 40.00	9.61- 9.64- 9.77-	3.0072 2.7929 2.6833	.0275- .0212- .0268-	•7958- •7957- •7553-	.0051- .0002 .0344	.0095- .0232- .0848-	•2441- •2225- •0217
110 110 110	246 246 246	1413 1414 1415	10.00 10.00 10.00	20.00- 20.00- 20.00-	15.00 30.00 100.00	9.44 9.46 9.63	3.42- 3.43- 3.48-	.6866 .7026 .7014	.0273 .0287 .0283	•1772- •1786- •1779-	.0048 .0050 .0051	.0328- .0321- .0307-	.0897 .0909 .0855
110 110 110	247		20.00 20.00 20.00	20.00- 20.00- 20.00-	15.00 30.00 100.00	18.96 19.02 19.36	6.74- 6.76- 6.88-	1.5452 1.4491 1.4636	.0157 .0162 .0162	•5122- •4779- •4795-	.0014- .0029- .0062-	•0295- •0295- •0253-	•1069 •1084 •0931
116 110 110	248 248 248		30.00 30.00 30.00	20.00- 20.00- 20.00-	15.16 30.32 101.06	28.60 28.71 29.23	9.88- 9.92- 10.07-	2.2518 2.2833 2.1998	.0048 .0133 .0065	.6618- .7225- .7043-	.0129 .0130 .0170	•0382- •0369- •0062	.0738- .0806- .0648-
110 110 110		1422 1423 1424	10.00 10.00 10.00	30.00- 30.00- 30.00-	15.00 30.00 100.00	8.70 8.73 8.86	4.99- 5.01- 5.08-	.6705 .6666 .6427	.0289 .0307 .0299	•1734- •1680- •1625-	.0041 .0060 .0062	•0362- •0417- •0438-	.0911 .1132 .1204
110 110 110			20.00 20.00 20.00	30.00- 30.00- 30.00-	15.00 30.00 100.00	17.55 17.61 17.87	9.87- 9.91- 10.05-	1.3421 1.3525 1.3390	.0185 .0213 .0193	•4271- •4412- •4399-	.0100 .0071 .0055	•0468- •0444- •0503-	•1377 •1443 •1528
110 110 110	251	1428 1429 1430	10.00 10.00 10.00	50.00- 50.00- 50.00-	15.00 30.00 100.00	6.47 6.48 6.53	7•66- 7•66- 7•72-	•5022 •4796 •4666	.0362 .0343 .0322	•1328- •1238- •1150-	.0038 .0045 .0050	•0767- •0750- •0757-	•2137 •2095 •2054
110 110 110	252 252 252	1431 1432 1433	26.00 26.00 26.00	50.00- 50.00- 50.00-	15.00 30.00 100.00	13.21	15.21- 15.24- 15.36-	•9557 •9445 •9479	.0191 .0168 .0173	•2794- •2795- •2886-	.0201 .0215 .0202	•1771- •1640- •1491-	•4436 •4377 •3999
110 110 110	253 253 253	1434 1435 1436	10.00 13.00 10.00	70.60- 70.60- 70.00-	15.00 30.00 100.00	3.45 3.45 3.46	9•40- 9•40- 9•42-	•2759 •2370 •2373	.0414 .0399 .0370	•0760~ •0594~ •0582~	.0033 .0026 .0022	•1090- •0997- •0968-	•2854 •2645 •2527
110 110 110	254 254 254	1437 1438 1439	10.00 10.00 16.00	90.60- 90.60- 90.60-	15.00 30.00 100.00	.00 .00	10.00- 10.00- 10.00-	.0464 .0207 .0070	.0472 .0434 .0419	.0142- .0081- .0044-	.0024- .0023- .0023-	•1082- •1036- •1017-	•2818 •2713 •2610
110		1440 1441 1442	30.00 30.00 30.00	5.00 5.00 5.00	15.16 30.32 101.06	30.03 30.17 30.76	2•51 2•52 2•56	2.3507 2.3113 2.3093	.0120- .0107- .0154-	•7860- •7945- •7901-	.0072- .0007- .0054-	•0180- •0212- •0192-	•0570 •0726 •0581
110	256	1443 1444 1445	40.00 40.00 40.00	5.00 5.00 5.00	15.34 30.68 102.25	40.05 40.21 40.96	3.22 3.23 3.28	2.8563 2.8203 2.8328	.0379- .0369- .0368-	.8053- .8360- .8897-	.0276- .0299- .0188-	.0075 .0132 .0119	.0259 .0521 .0091
110	257	1446 1447 1448	50.00 50.00 50.00	5.00 5.00 5.00	15.57 31.15 103.82	50.06 50.21 50.97	3 • 8 4 3 • 8 4 3 • 8 9	3.0133 2.8128 2.8177	.0297- .0274- .0292-	.6011- .6731- .7778-	.0214- .0167- .0037-	.0453 .0345 .0334	•0111 •0347- •0579-
110	258		60.00 60.00	5.00 5.00 5.00	15.83 31.65 105.50	60.08 60.23 61.05	4.33 4.34 4.38	3.0690 2.8289 2.9593	.0331- .0361- .0353-	.6384- .6455- .8757-	.0102- .0060- .0067-	.0633 .0483 .0079	•0243- •0392- •0986-
116	259	1452 1453 1454	70.60 70.00 70.00	5.00 5.00 5.00	16.13 32.25 107.50	70.11 70.28 71.10	4.70 4.71 4.73	3.0583 2.9357 2.9421	.0266- .0235- .0196-	.8417- 1.0146- 1.1346-	.0063- .0075- .0090-	.0055- .0240 .0081-	.0910- .0718- .1078-
110	260		80.00 80.00 80.00	5.00 5.00 5.00	16.22 32.43 108.10	80.16 80.32 81.15		3.1730 2.9516 2.9542	.0133- .0187- .0243-	1.1724- 1.2160- 1.3401-	.0063- .0073- .0076-	.0001 .0098 .0006	•1471- •1284- •1218-
110		1459	90.00 96.00 96.00	5.00 5.00 5.00	16.28 32.55 108.50	90.18 90.36 91.17	5.00	3.0036 2.9606 2.9123		1.6146- 1.6577- 1.7132-	.0046- .0051- .0048-	•0141- •0027 •0125	•1843- •1555- •1062-
110	262	1462	10.00 10.00 10.00	10.60 10.60 10.60	15.00 30.00 100.00	9.88 9.92 10.11	1.74 1.74 1.77	•7625 •7448 •7434	•0242 •0264 •0270	•1841- •1869- •1901-	.0024- .0024- .0025-	.0186 .0209 .0161	•0616 - •0640- •0453-
110	263	1465	20.00 20.00 20.00	10.00 10.00 10.00	15.00 30.00 100.00	19.80 19.88 26.27	3.43	1.5530 1.4571 1.5228	.0095 .0122 .0118	•4959- •4903- •4958-	.0008 .0027 .0027	.0215 .0141 .0099	•0770- •0572- •0356-
116	264	1468	36.00 36.00 30.00	10.00 10.00 10.00	30.32	29.75 29.88 30.47	5.02	2.3340 2.3475 2.2994	.0155- .0096- .0219-	.7503- .7893- .7761-	.0036- .0004- .0070-	.0068- .0182- .0187-	.0617 .0851 .0880
110 .	265	1471	40.00 40.00 40.00	10.00 10.00 10.00		39.72 39.89 40.61	6 • 4 5	2.9063 2.9094 2.7992	.0467- .0430- .0346-	.7877- .8403- .8535-	.0318- .0212- .0308-	.0379 .0330 .0299	.0187 .1031 .0101-

 $^{{}^{\}dagger}\mathbf{M}\text{inus signs}$ are to the right of the numbers to which they apply.

TABLE III. - AERODYNAMIC COEFFICIENTS OF MODEL FOR THE COMPLETE INVESTIGATION - Continued

Config.	Run	Point	α ₁ , deg	ø, deg	q, lb/sq ft	α, deg	β, deg	c _N	C _A	C _m	c,	Cn	CY
115	266	1473	50.00	10.00	15.57	49.74	7.66	2.9594	.0419-	•5356-	.0131-	.0684	.0086-
115	266	1474	50.00	10.60	31.15	49.92	7.68	3.1134	.1509-	1•2729-	.0211-	.2749	.1851-
116	266	1475	50.00	10.60	103.82	50.61	7.76	2.7480	.0308-	•7554-	.0009	.0608	.1059-
110	267		60.00	10.00	15.83	59.79	8.66	2.8928	.0367-	•5530-	.0076-	•1315	•0652-
110	267		60.00	10.00	31.65	59.95	8.67	2.8908	.0119-	•6276-	.0096-	•1120	•0812-
110	267		60.00	10.00	105.50	60.16	8.69	1.4044	.0237-	•0452-	.0198-	•0179	•2032-
110	268	1479	76.00	10.00	16.13	69.90	9.40	3.1260	.0278-	•8856-	.0418-	•0222	•1968-
110	268	1480	70.06	10.00	32.25	70.66	9.41	2.8962	.0291-	•9641-	.0160-	•0399	•1787-
110	268	1481	76.00	10.00	107.50	70.84	9.45	2.8414	.0221-	1•0824-	.0178-	•0173	•2154-
110	269	1482	80.00	10.00	16.22	80.64	9 • 8 5	3.0707	.0168-	1.1525-	.0147-	•0012-	•2741-
110	269	1483	80.00	10.00	32.43	80.19	9 • 8 5	2.8203	.0216-	1.1675-	.0140-	•0019-	•2272-
110	269	1464	80.00	10.00	108.10	86.98	9 • 8 8	2.8225	.0225-	1.2740-	.0138-	•0063	•2326-
110	270	1485	96.00	10.00	16.28	90.17	16.00	2.8699	.0000	1.5863-	.0064-	.0257-	•3200-
110	270	1486	96.06	10.00	32.55	90.33	10.00	2.8161	.0138-	1.6245-	.0075-	.0082	•2604-
110	270	1487	96.06	10.00	108.50	91.17	10.00	2.9066	.6177-	1.7194-	.0080-	.0294	•2309-
110 110 116			26.00 26.00 26.00	15.00 15.00 15.00	15.00 30.00 100.00	19.46 19.53 19.90	5.10 5.11 5.21	1.6221 1.4519 1.5426	.0114 .0134 .0136	•5375- •4905- •4993-	.0038 .0060 .0072	•0285 •0163 •0155	.0983- .0735- .0584-
110 110 115	272	1491 1492 1493	36.00 36.00	15.60 15.60 15.60	15.16 30.32 101.06	29.27 29.40 29.95	7.46 7.49 7.62	2.4789 2.3581 2.2638	.0352- .0316- .0344-	•7909- •7785- •7547-	.0025- .0045- .0060-	•0013 •0007- •0229-	•1054 •0973 •1120
110	273	1494	46.00	15.00	15.34	39.17	9.60	2.8071	.0300-	.7481-	.0029-	•0177	•2227
116	273	1495	46.00	15.00	30.68	39.32	9.63	2.7733	.0305-	.7820-	.0029-	•0309	•1974
115	273	1496	46.00	15.00	102.25	40.01	9.77	2.7163	.0324-	.7922-	.0334-	•0779	•0291-
110	274		10.00	20.00	15.00	9.44	3.42	.6967	.0269	•1554-	.0028-	•0287	.0731-
114	274		10.00	20.00	30.00	9.46	3.43	.6797	.0265	•1651-	.0043-	•0258	.0686-
110	274		10.00	20.00	100.00	9.63	3.48	.7021	.0272	•1783-	.0048-	•0274	.0747-
110 110 110	275		20.00 20.00 20.00	20.60 20.60 20.60	15.00 30.00 100.00	18.96 19.02 19.36	6•74 6•76 6•88	1.5340 1.4128 1.4721	+0142 +0156 +0153	•4936- •4564- •4667-	.0037 .0049 .0084	•0256 •0247 •0175	.0778- .0760- .0759-
110		1504	30.00	20.60	15.16	28.60	9.88	2.3246	•0150	.6823-	.0111-	.0094	•1335
110		1504	30.00	20.66	30.32	28.71	9.92	2.2428	•0162	.7200-	.0110-	.0081	•1076
110		1505	30.00	20.66	101.06	29.25	10.08	2.2507	•0129-	.8947-	.0139-	.0199-	•1007
110	277	1506	10.00	30.00	15.00	8.70	4.99	.7206	.0287	•1818-	.0063-	.0548	•1457-
110	277	1507	10.00	30.00	30.00	8.73	5.01	.6496	.0272	•1698-	.0062-	.0500	•1361-
110	277	1508	10.00	30.00	100.00	8.86	5.08	.6537	.0284	•1676-	.0063-	.0455	•1248-
110		1509	20.00	30.00	15.00	17.55	9.87	1.3442	.0215	.3000-	.0111-	•0674	•1916-
110		1510	20.00	30.00	30.00	17.61	9.91	1.3402	.0194	.4388-	.0077-	•0529	•1615-
110		1511	20.00	30.00	100.00	17.88	16.65	1.3677	.0271	.4482-	.0038-	•0529	•1554-
110	279	1512	10.00	50.00	15.00	6.47	7.66	.4986	.0316	•1281-	.0048-	•0794	•2161~
110		1513	10.00	50.00	30.00	6.48	7.66	.4784	.0355	•1186-	.0193-	•0738	•1995~
110		1514	10.00	50.00	100.00	6.54	7.73	.4868	.0301	•1230-	.0049-	•0727	•1967~
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 $^{^{\}dagger}$ Minus signs are to the right of the numbers to which they apply.

TABLE III. - AERODYNAMIC COEFFICIENTS OF MODEL FOR THE COMPLETE INVESTIGATION - Continued

Config.	Run	Point	α ₁ , deg	ø, deg	q, lb/sqft	a, deg	β, deg	C _N	C _A	C _m	c,	Cn	C¥
110	280	1515 1516 1517	20.00 20.00 20.00	50.00 50.00 50.00	15.00 30.00 100.00	13.19 13.21 13.32	15.22 15.24 15.36	1.0116 .9667 .9706	.0122 .0130 .0135	•3125- •3023- •3047-	.0236- .0186- .0199-	•1622 •1513 •1450	•4314- •4134- •3930-
110	281	1518 1519 1520	10.00 10.00 10.00	70.00 70.00 70.60	15.00 30.00 100.00	3.45 3.45 3.46	9.39 9.40 9.42	.2547 .2270 .2395	•0382 •0379 •0357	.0601- .0467- .0604-	.0045 .0014 .0004-	•0999 •0957 •0940	•2678- •2503- •2485-
110	282	1521 1522 1523	10.00 10.00 10.00	90.60 90.60 90.60	15.00 30.00 100.00	.00	10.00 10.00 10.00	.0080 .0064 .0081	.0450 .0419 .0409	.0026- .0030- .0073-	.0018 .0028 .0032	•1087 •1022 •1082	•2722- •2561- •2619-
		1546 1547	70.00 80.00	15.00 15.00	16.13	69.53 79.82	14.09 14.77	2.9747 2.8198	.0368- .0163-	-8063- 1-0619-	.0179- .0159-	-0904 -0544	•2536- •2990-
		1635 1636	70.03 80.00	10.00- 10.00-	16.13 16.22	69.89 80.03	9.40- 9.85-	2.9007 2.9145	•0547- •0086-	•7686- 1•1139-	.0364 .0173	•0567 •0746-	•3405 •3621
		1637 1638	70.00 80.00	15.00- 15.00-	16.13 16.22	69.51 79.82	14.09- 14.77-	2.8542 2.6993	.0509- .0008	•7532- 1•0706-	•0254 •0222	•0421 •0056	•5266 •4534
		1639 1640	70.00 80.00	10.00 10.00	16.13 16.22	69.90 80.03	9•40 9•85	3.0832 2.9126	.0391- .0082-	.8752- 1.1267-	.0192- .0170-	•0306- •0247-	•2859- •3125-
		1651 1652	70.00 80.00	10.00- 10.00-	16.13 16.22	69.89 80.04	9.40- 9.85-	2.9222 2.9737	.0402- .0123-	.8159- 1.1364-	.0148 .0172	.0528 .0167	•3133 •2969
146 146	331 331	1669 1670 1671 1672	50.00 60.00 70.00 80.00	5.00 5.00 5.00 5.00	15.57 15.83 16.13 16.22	50.06 60.07 70.12 80.15	3.84 4.33 4.70 4.92	2.9063 2.9862 3.1538 3.0539	.0220- .0460- .0406- .0301-	.6838- .5067- .9438- 1.1052-	.0115 .0028 .0003- .0032-	•0290- •2738 •1394 •0722	.0535- .2287 .0791 .0227-
140 140	332 332	1674 1675	50.00 60.00 70.00 80.00	10.00 10.00 10.00	15.57 15.83 16.13 16.22	49.74 59.79 69.90 80.04	7•66 8•66 9•40 9•85	3.0114 3.0268 3.1045 3.0409	.0149- .0476- .0424- .0286-	.7343- .5246- .9157- 1.1351-	.0060 .0043- .0097- .0110-	.0624- .2100 .1422 .0590	.0757- .0770 .0136- .1435-
140 140	333	1678 1679	50.00 60.00 70.00 80.00	15.00 15.00 15.00	15.57 15.83 16.13 16.22	49.19 59.28 69.51 79.82	11.46 12.97 14.09 14.77	3.0910 2.7069 2.8320 2.7914	.0144- .0146- .0372- .0078-	•7225- •7432- •7772- 1•0960-	.0041 .0154- .0187- .0141-	•1547- •0930- •0576 •0598	•1631- •4716- •2921- •2866-
140 140	334 334	1681 1682 1683 1684	50.00 60.00 70.00 80.00	.00 .00 .00	15.57 15.83 16.13 16.22	50.18 60.17 76.19 80.19		3.1173 2.9553 3.1196 3.0739	.0453- .0331- .0351- .0216-	.5734- .7292- .9766- 1.1244-	.0056- .0016 .0039 .0024	.0534- .0489 .0039 .0326	.0050 .0936 .0279 .0581
		1653 1654	70.00 80.00	10.00 10.60	16.13 16.22	69.90 80.03	9•40 9•85	3.0129 2.9208	.0390~ .0116~	.8911- 1.1311-	.0178- .0169-	•0143- •0116-	•2656- •2957-
		1655 1656	76.00 86.00	15.00 15.00	16•13 16•22	69.51 79.82	14.09 14.77	2.8299 2.8356	.0408- .0005-	.8016- 1.2582-	.0255- .0190-	.0294- .0118-	•4321- •3833-
150	328	1657 1659 1660	50.00 70.00 80.00	5.00- 5.00- 5.00-	15.57 16.13 16.22	50.06 70.11 80.16		2.9497 3.0834 3.0969	.0188- .0393- .0228-	•6461- •9316- 1•1556-	.0092- .0075 .0054	•0568- •0276- •0760-	.0579- .1333 .0984
150 150	329 329	1661 1662 1663 1664	50.00 60.00 70.00 80.00	10.60- 10.00- 10.00- 10.00-	15.57 15.83 16.13 16.22	49.74 59.79 69.89 80.04	8•66- 9•40-	3.0918 3.0001 2.9437 3.0093	.0475+ .0386- .0450- .0304-	.5821- .6409- .8174- 1.1072-	.0042 .0149 .0141 .0140	.0587 .0320- .0955- .0663-	•1530 •1887 •1090 •1971
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 $^{^{\}dagger}$ Minus signs are to the right of the numbers to which they apply .

TABLE III. - AERODYNAMIC COEFFICIENTS OF MODEL FOR THE COMPLETE INVESTIGATION - Continued

Config.	Run	Point	α ₁ , deg	ø, deg	q, lb/sqft	α, deg	β, deg	c _N	С А	C _m	c ₁	Cn	CY
150	330	1665	50.00	15.00-	15.57	49.18	11-46-	2.9051	.(435-	.5678-	-0080	-1431	•3217
150	330	1666	60.00	15.00-	15.83	59.29	12-97-	2.8304	(355-	+6469-	.0194	•0746	•4292
150 150	330 330	1667 1668	70.00 80.00	15.00-	16.13 16.22	69.53 79.82	14-09-	2.8886	.(452-	1.1033-	•0205 •0157	•0637- •0869-	•3416 •3221
	1	i		ļ		ł	İ	l	1	i	ļ	i	
150 . 150	335 335	1685 1686	50.00 60.00	•00	15.57	50.18 60.18	•00	3.1205	.0384-	•6344- •7346-	.0020	•0730- •0224-	•2145- •0603-
150	335	1687	70.00	00	16.13	70.19	•00	3.1478	.6450-	1.0197-	.0045-	-2099-	2990-
150	335	1688	80.00	•00	16.22	80.20	•00	3.0800	.0217-	1.1710-	-0006-	-0435-	.0649-
160	283	1524	80.00	15.00	16.22	79.84	14.77	2.9086	.0319-	1.1097-	.0178-	-0060	.4407-
160	284	1525	80.00	15.00-	16.22	79.82	14.77-	2.8149	.0012	1.3598-	.0121	-0970-	.2999
160	289	1540	70.00	15.00-	16+13	69.51	14.09-	2.8120	.(436-	.8783-	.0211	-0265-	.3819
160	289	1541	70.00	15.00-	21.50	69.57	14.09-	2.7855	.(410-	•9587-	.0219	-0141-	•4035
160	290	1542	70.00	15.00	16+13	69.51	14.09	2.7871	•6431-	.9674-	.0207-	-0844-	.5594-
160	291	1542	70.00	15.00-	16.13	69.53	14.09-	2.8913	.0441-	•9126-	.0222	•0259-	-3812
176	292	1543	70.00	15.40-	16+13	69.53	14.09-	2.8765	.0472~	-9731-	.0219	.0468	-5655
170	293	1544	70.00	15.00	16.13	69.51	14.09	2.8078	.0406-	.8969-	-0216-	•0095	•3634-
206	104	620	.00	•00	15.00	.00	.00	.0614	.0092	.0355-	.0000	.0057	•0236-
200	164	621	•00		20.00	.00	•00	.0332	.0071	.0154-	.0000	.0051	.0184-
	164	622	•00	•60	30.00	•00	•00	.0299	•6080	-0120-	•0006	.0031	+0145-
200	104	623	-00	-00	40.00	.00	•00	.0093	.0079	•0007-	-0004	•0024	•0096-
200 200	104 164	624 625	.0u	.00	100.00	.00	•00	.0061	.0082 .0083	.0016 .0018-	.0004	.0019 .0011	-0067- -0045-
	_							1	1				
200	105	626	10.00	•00	15.00	10.01	•00	•1610	•0071	.0382	.0009	•0060	•0247-
	105 105	627 628	10.00 10.00	.00	20.00 30.00	10.01	•00	.1710 .1388	.C381 .C376	.0410 .0499	.0010	+0022 +0026	.0139- .0126-
200	105	629	10.00		40.00	10.01	.00	.1358	.0375	.0501	.0006	.0014	-0800-
200	105	63C	10.00		60.00	10.02	•00	.1241	.0378	.0598	.0005	.0010	.0043-
200	165	631	10.30	•00	100.00	10.04	••0	.1250	*C281	.0574	.0005	•0009	-0023-
260	106	632	20.00	•00	15.00	20.02	•00	.4479	.0333-	.0089-	.0039	-0051-	-8000
260	106 106	633 634	20.00	•60 •66	20.00 30.00	20.03	•00	.4397 .4209	.C320-	.0119-	.0024	.0044- .0028-	•0011
200	166	635	20.00	.00	40.00	20.06	.00	4381	-0550-	.0125-	.0020	.0018-	•0039
200	106	636	20.00	.00	60.00	20.69	•00	.4240	.0028-	.0031-	.0016	.U008-	.0014
200	106	637	20.00		100.00	20.16	•00	.4253	.C029-	•0107	.0014	•0003	.0013
200	107	638	30.00	•60	15.16	30.06	•00	.9916	-0256-	•0927-	•0011	-0176-	.0463
	107	639	30.00	•00	20.21	30.07	-00	9477	-0254-	-1291-	•0006	.0343-	•0954
	107 107	640 641	30.00 30.00	•00	30.32 40.42	30.09 30.12	•00	.8429 .8210	•0274- •0269-	•1110- •0907-	•0047 •0048	.0088 .0199	•0148- •0549-
	107	642	30.00	.60	60.64	30.18	•00	.8209	-8850	-0666-	.0030	.0038-	.0103
	107	643	30.00	•60	101.06	30.31	•00	.8379	.0292-	.0471-	•0015	-0122-	•0300
	108 108	644 645	40.00 40.00	•0u	15.34 20.45	40.09 40.12	•00	1.5405	-0240-	.0201	.0119	•0642	•40∠7-
	108	646	40.00	.00	30.68	40.15	•00	1.5214	-0265- -0520-	.0508- .1109-	.0109 .0037	•0723 •0062	•3608- •0302-
	108	647	40.00	•00	40.90	40.19	•00	1.2543	.0,53-	1398-	.0047	.0433	-1059-
200	109	650	50.00	•00	15.57	50.10	•00	1.7886	.0.01-	-0600-	.0072	-2444-	.3447-
200	109	651	50.00	•QU	20.76	50.13	•00	1.6999	-0738-	•0739	-0080	-0874-	•3424-
	109	652	50.00	•60	31.15	50.18	-00	1.5740	•0351-1	-0632-	.0003-	-0354-	•0213
200	169	653 654	50.00 50.00	.00 .00	41.53 62.29	50.23 50.34	•00	1.4929	.0379- .0391-	•1128- •1452-	.0011 .0023	•0247 •0607	•0150 •0029
20.	110	656	60.00	•00	15.83	60.11	•00	1.8215	.0714-	.1444	.0026	-0220-	-1300-
	110	657	60.0u	•00	21.10	60.13		1.6643	.0321-	.1316	.0015	•0567	0788
	110	658 659	60.00	• U Ü	31.65 42.20	60.19 . 60.25	•00	1.6324	.0319- .0369-	•0636- •1265-	.0038	-1013	-1106
	110	660	60.00	.00	63.30	60.37		1.5737	0168-	1618-	.00∠4	•0778 •0679	•0958 •0707
	110	661	60.00	.00	105.50	60.60		1.5235	0110-	1312-	.0011-	.0426	.0085
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 $^{^{\}dagger}$ Minus signs are to the right of the numbers to which they apply.

TABLE III. - AERODYNAMIC COEFFICIENTS OF MODEL FOR THE COMPLETE INVESTIGATION - Continued

Config.	Run	Point	α ₁ , deg	ø, deg	q, lb/sqft	α, deg	β, deg	C _N	C _A	C _m	cı	Cn	C _¥
260	111	662	70.00	•60	16.13	70.10	•00	1.6712	.0672-	.0170-	•0014	•1097	•0706
200	111	663	70.CU	•60	21.50	70.13	•00	1.6091	0746-	.0047- .0854-	.0021 .0018	•1806 •1825	•1633 •2076
200	111	664	70.00 70.00	•ÇÜ	32.25 43.00	70.19 70.24	•00 •00	1.5908	.0787-	.1490-	.0008	•1275	.1259
200	111	665 666	70.00	•60	64.50	70.37		1.5554	.0887-	1851-	.0012	.0847	.0666
200	111	667	70.00	03.	107.50	70.60	•00	1.5648	.0904-	.1877-	•0007	.0553	.0390
250	112	668	80.00	•60	16.22	80.11	-00	1.6081	.0474-	.1253-	•0013	•0191	.0726-
20C	112	669	80.00	•00	21.62	80.13	•00	1.5596	.0494- .0544-	•1133- •1719-	.0015 .0011	.0133 .0214	•0677- •0256-
200	112	670	80.00 80.00	•00	32.43 43.24	80.19 80.24	•00	1.5166	.0573-	.2292-	•0012	.0228	.0143-
250 200	112 112	671 672	80.00	.60	64.86	Bu . 36	•00	1.4958	0656-	2912-	.0009	.0215	.0034-
200	112	د 67	86.00		108.10	80.59	•00	1+4541	•0667-	•3205~	•0007	•0053	•0054-
200	113	674	96.00	.00	16.28	90.10		1.6059	.0039	.4247-	•0000	-0124-	.0092-
200	113	675	90.00	.00	21.70	90.12		1.5031	•0017	•4105-	.0005	.0149-	•0023 •0077-
200 .	113	676	90.00	•00	32.55 43.40	90.18	•00	1.4841	.0160- .0322-	•4369- •4447-	•0003 •0004	.0149- .0167	.0430
200	113 113	677 678	90.00	•00	65.10	90.25	•00	1.4357	0380-	.4798-	.0003	•0003	.0366
200	113	679	90.00	.00	108.50	90.56	.00	1.3971	.0460-	.5108-	.0004	.0154	.0498
200	114	680	.0.	5.60-	15.00	.00	••¢	.0064-	.0069	.0105	.0011-	-0067	.0249~
200	114	681	-00	5.00-	20.00		•00	.0054-	•0077	-0102	.0004-	-0051	•0190-
200	114	682	-00	5.00-	30.00	.00	•00	•0037-	•0081	.0095	.0003-	.0035	-0129-
200	114	683	.00	5.00-	40.00	•00	••0	.0027- .0019-	.0071 .0073	.0101	.0002- .0000	.0031 .0024	.0101-
200	114	684 685	.00 .00	5.00- 5.00-	60.00 100.00	.00	•00	.0010-	.0072	.0080	.0000	.0015	.0029-
200	115	686	10.00	5.00-	15.00	9.97	•87-	.0957	.0047	.0802	.0001-	.0127	.0266-
200	115	687	10.00	5.00-	20.00	9.97	-87-	.0969	•0060	.0744	.0003	•0112	-0227-
200	115	688	16.00	5.60-	30.00	9.97	-87-	.1163	•0070	.0693	.0004	•0100	-0145-
200	115	689	10.00	5.40-	40.00	9.97	•87−	•1065	•0075	.0706	.0003	-0095	-0138-
200 200	115 115	690 691	10.00 10.00	5.00- 5.00-	60.00 100.60	9.98 10.00	•87- •87-	.1135 .1144	•0076 •0074	.0685 .0634	.0006	•0079 •0061	.0083-
200	116	692	20.00	5.00-	15.00	19.95	1.71-	.4345	.0073-	.0118	•0073	-0210	.0275-
200	116	693	26.00	5.60-	20.00	19.96	1.71-	.4087	.0049-	.0116	.0019	-0182	.0161-
20C	116	693	20.00	5.CU-	30.00	19.97	1.71-	•4031	.0047-	.0037	.0014	•0166	.0068-
200	116	694	20.00	5.60-	40.00	19.99	1.71-	+3863	.0041- .0044-	•0115	+0018	-0145	.0014
200 200	116	695 696	20.00 20.00	5.60- 5.66-	100.00	20.02	1+72- 1+72-	.4086 .4128	.0044-	.0030	.0020 .0042	.0118 .0118	.0091
260	117	697	36.00	5.00-	15.16	29.96	2.50~	.9168	.0303-	.0458-	.0034	•0325	.0137-
200	117	698	30.00	5.00~	20.21	29.97	2.50-	9210	.0296-	.1046-	.0041	.0445	-0400-
200	117	699	30.CU	5.00-	30.32	30.00	2.50-	8534	•0252~	•1239-	•0069	•0875	-1681-
20C	117	700	30.00	5.00-	40.42	30.03	2.51-	.8121	•0236-	-1141-	•0070	+0845	-1690-
200 200	117 117	701 702	30.00	5.00- 5.00-	101.06	30.09	2•51- 2•52-	.8322 .8327	•0244- •0295-	•1138- •0823-	.0060 .0053	.0708 .0420	•1268- •0322-
	1	703	40.00	5.00-		39.98	3.22-	1.5064	.0409-	.0269-	.0151	.1114	.4251-
200 200	118	704	40.00	5.00-	15.34 20.45	40.00	3.22-	1.4589	0397-	.1453-	.0176	1119	4545-
200	118	705	40.00	5.00~	30.68	40.04	3.22-	1.3354	.0476-	.1818-	.0132	.1220	-3135-
200	118	7∪6	40.00	5.00-	40.90	40.08	3 - 22-	1.2673	.0473-	-2146-	.0136	•1158	-3264-
260 260	118 118	707 708	40.00 40.00	5.00-	61.35	40.18	3.23-	1.2832	.0455- .0466-	•2374- •2003-	.0148 .0147	•1275 •1211	-3494- -3292-
			Ì		ł		1				.0115	.0721-	.2905-
200 200	119 119	709 716	50.00 50.00	5.00- 5.00-	15.57	49.99 50.02		1.7185	.0629~ .0704~	.0684 .0145	.0146	•0158	.2743-
200	119	711	50.00	5.CU-	31.15	50.07		1.5373	.0778-	•1172-	.0108	•0938	-0890-
200	119	712	50.00	5.00-	41.53	50.12		1.5329	-0829-	-1852-	.0110	•1220	-0610-
200	119	713	50.00	5.00-	62.29	50.24	3.85~	1.5142	-0804-	.1980-	•0130	+1127	-1058-
200	119	714	50.00	5.00~	103.82	50.47	3.86-	1.5219	.0785-	-1839-	•0119	+0853	-1280-
200	120	715	60.00	5.00-	15.83	60.00	4.33-	1.7283	-0843-	-1411	•0059	•2233	-3169
200	120	716	60.CL	5.00-	21.10	60.03		1.6888	.0918- .0980-	•0464 •0619-	.0065 .0073	•2478 •2194	•3724 •2948
200 200	120	717 718	60.0U	5.00- 5.00-	31.65	60.09		1.5578	.0933-		.0068	•1816	.2543
200 200	120	719	60.CL	5.00-	63.30	60.26		1.5427	.0990-	.1321-		•0599	.0664
200	120	720	60.00		105.50	60.51		1.5668	.0992-	•1254-		•0023	•0107-
200	121	721	70.00	5.CU-	16.13	76.03		1.6204	-0821-	.0001-		.2003	-2451
200	121	722	70.00	5.00-	21.50	70.65		1.5632	.0835- .0815-	.0423- .1059-	.0049 .0059	•2245 •2162	•3101 •3084
260 266	121	723	70.00	5.00- 5.00-	32.25 43.00	70.12 70.17		1.5598	.0800-	•1059- •1599-	.0055	•1427	.2230
200	121	724 725	70.00	5.60-	64.50	70.29		1.5302	-0857-	2024-	.0059	-0480	.0971
200	121	726	70.00	5.00-	107.50	70.53		1.5084	.0894-	.2106-	-0058	•0317	.0126-
200	122	727	Bu.00	5.40-	16.22	80.07		1.7039	•0605-	•1286-		-0361	.0328
200	122	728	80.00	5.00-	21.62	80.10		1.5778	0634-	•0951- 1727-	•0047	-0312	-0461
200	122	729	80.00	5.00- 5.00-	32.43 43.24	80.15		1.4860	•0643- •0674-	•1727- •2244-	.0054 .0057	.0128 .0027	.0417 .0530
						BUALL			/				
200	122	730 731	80.00	5.00-	64.86	80.32	4.93-	1.4507	.0627-	.2854-	.0060	.0032	.0557

 $^{{}^{\}dagger}\text{Minus signs}$ are to the right of the numbers to which they apply.

TABLE III. - AERODYNAMIC COEFFICIENTS OF MODEL FOR THE COMPLETE INVESTIGATION - Continued

Config.	Run	Point	α ₁ , deg	ø, deg	q, lb/sq ft	α, deg	β, deg	c _N	C _A	C _m	c,	Cn	C¥
200	123	733	90.00	5.00-	16.28	90.09	5.00-	1.5151	.0031-			-0364	-0098
200 200	123	734 735	96.00 96.00	5.00-	21.70 32.55	90.13	5.00-	1.5722	.0100-	•4397- •4396-	.0040	•0073 •0220	•0398 •0203
200	123	736	96.00	5.00-	43.40	96.23	5.00-	1.4226	.0230-	-4307-		-0124-	.0248
200	123	737	90.00	5.00-	65.10	90.35	5.00-	1.4496	.0376-		-0058	.0056-	.0617
200	123	738	90.00	5.00-	108.50	90.56	5.00-	1.4035	.0430-			-0054	.0825
200	124	739	.00	10.66-	15.00			.0271	.0648	.0111-	.0011	.0025	-8600
20C	124	740	•00	10.00~	20.00	•00	•00	.0058-		د6006ء	.0008	.0018	-1000-
200	124	741	.00	10.66-	30.00	.60		.0135	•6071	.0014-	.0006	•0013	.0023-
200	124	742	-00	10.00-	40.00	.00	•00	.0027-	•0068	.0091	.0004	0018	.0023-
200 200	124	743 744	.0u	10.60-	100.00	.00	.00	.0022	.0074 .0073	.0052	.0004	.0010 .0003	.0016-
200	125	745	10.00	10.00-	15.00	9.86	1.73-	.1142	•0073	.0698	.0021	.0107	.0039
200	125	746	10.00	10.00-	20.00	9.86	1.73-	1371	.0060	.0579	.0025	0122	0007-
200	125	747	10.00	10.60-	30.00	9.86	1.73-	1177	.0069	0617	.0016	0103	-0011
200	125	748	10.00	10.00-	40.00	9.86	1.73-	.1080	.0079	.0687	.0013	•0093	.0051
200	125	749	10.00	10.65-	60.00	9.87	1.73-	1195	•0075	.0631	.0013	•0101	-0016
200	125	750	10.00	10.00-	100.00	9.88	1.74-	.1157	•0076	.0618	•0011	•0082	•0055
200	126	751	20.00	10.00-	15.00	19.74	3.41-	.4310	-0016-		.0031	-0201	.0281
200	126	752	20.00	10.00-	20.00	19.75	3-41-	•4277	-0018-	.0091-	.0040	•0215	•0293
200	126	753	20.00	10.00-	30.00	19.76	3 • 41 -	3911	-0028-	.0031-	-0032	•0206	-0288
20C 20C	126	754 755	20.66	10.00-	60.00	19.78	3.41-	-3849	•0029-	.0083	-0029	•0174	•0353
200	126 126	756	20.00 20.00	10.00-	100.00	19.81	3.42-	.3913 .3895	.0032- .0027-	.0160 .0185	.0034 .0031	•0155 •0153	-0412 -0435
200	127	757	30.00	10.00-	15.16	29.67	4.99-	.9420	.0191-	.0684-	.0090	-0856	.0830-
200	127	758	30.00	10.66-	20.21	29.69	4.99-	9015	.0184-	.1162-	0091	-0834	-0834~
206	127	759	30.00	10.00-	30.32	29.71	4.99-	.8233	.0163-	-1408-	.0113	-1063	-1694-
206	127	760	30.00	10.00-	40.42	29.74	5.00-	.8369	.0177-	•1432-	.0114	+1099	-1801-
200	127	761	30.00	10.00-	60.64	29.81	5.01-	.6384	.0182-	•1339-	.0108	•1091	-1704-
20C	127	762	30.00	10.00-	101.06	29.93	5.02-	.8366	.0256-	•1021-	.0065	-0763	•0166-
200 200	128 128	763 764	40.00 40.00	10.00-	15.34	39.64	6-42-	1.4924	.0318-	-1114-		+1289	-3118-
200	128	765	40.00	10.00-	20.45 30.68	39.67 39.70	6.42-	1.2590	•0190- •0353-	-1889-		•1212	•3362-
200	128	766	40.00	10.00-	40.90	39.75	6.43-	1.2997	.0373-	•1656- •2475-	.0216 .0199	•1029 •1063	•3710- •3363-
200	128	767	40.00	10.00-	61.35	39.85	6.44-	1.2986	0395-	-2562-	.0215	-1103	.3452-
205	128	768	40.00	10.00-	102.25	40.05	6.47-	1.3134	.0394-		.0224	.0939	.3293-
206	129	769	50.00	10.00-	15.57	49.66	7.65-	1.6715	.0640-	•1672	.0190	-1463	.0775
	129	776	50.00 50.00	10.00-	20.76	49.70	7.66-	1.7029	-0600-	.0388	0205	.1510	-0018
	129	771		10.00-	31.15	49.73	7.66-	1.4451	-0620-	• U974-	.0165	•1122	-0065
	129	772	50.00	10.00-	41.53	49.79	7.67-	1.4656	-0705-	-1778-	-0181	•1311	+0294-
	129	773 774	50.00 50.00	16.66- 10.66-	62.29 103.82	49.91 50.12	7.68-	1.4966	.0723- .0727-	•2021- •1512-	.0192 .0175	•1077 •0646	.0937- .1209-
												1	i l
	130	775 776	60.00 60.00	10.00- 10.00-	15.83 21.10	59.72 59.74	8.65-	1.6756	•0714- •0787-	.0506 .0354	.0132	+2491	•4757
	130	777	60.00	10.00-	31.65	59.80	8.66-	1.5416	.0964-	•0554-	.0112 .0129	+2343 +2465	•4291 •4257
	130	778	60.00	10.60-	42.20	59.85	8.67-	1.4912	0964-	•1119~	.0128	•2126	•3459
	130	779	60.00	10.00-	63.30	59.96	8 • 68-	1.4931	0894-	-1305-	.0130	.0907	-1412
200	130	786	60.00	10.00-	105.50	60.20	8.70-	1.5126	.0400-	.1110-	•0111	.0220	.0244
	131	781	70.00	10.60-	16.13	69.80	9.39-	1.5154	•0666-	.0383	.0105	•1900	-3692
	131	782	70.00	10.00-	21.50	69.84	9.40-	1.5256	•0730-	.0495-	-0114	-2496	•4414
	131	783	70.00	10.60-	32.25	69.89	9.40-	1.4641	•0703-	.1032-	.0129	•2479	•4376
	131	784 785	70.00	10.60-	43.00 64.50	70.06	9.40- 9.41-	1.4277	•0393- •0809-	.1473-		-1582	•3387
	131	786	70.00	10.00-	107.50	70.29		1.4421	-0867-	•1762- •1813-		•0501 •0127	•1927 •1334
200	132	787	80.00	10.00-	16.22	79.95	9.85-	1.5193	.0464-	.0504-		-0547	.1886
	132	788	80.00	10.00-	21.62			1.5445	.0573-	.0634-		.0682	.1778
	132	789	80.00	10.60-	32.43	80.03	9.85-	1.4042	.0556-	.1144-	.0109	.0238	1682
200	132	790	86.00	10.60-	43.24	80.09	9.85-	1.4349	-0550-	-1911-	.0118	•0033	•1490
	132	791	80.00	10.00-	64.86	80.20	9.85-	1.4377	.0607-	.2594-	.0117	+0046	•1529
200	132	792	80.06	10.60-	108.10		9.86-		•0651-	•2819-	•0110	-0115	•1494
	133		90.00	10.60-	16.28	90.09	10.00- 10.00- 10.00-	1.4983	.0061	•3717- •3741-	.0092	-0581	•2093
	133		90.00 90.00	10.60-	21.70 32.55	90.12	10.00-	1.5221	•0002-	•3741-	•0098	•0479	-2036
	133		90.00	10.60-	43.40	90.17	10.00-	1.4102	.0088- .0219-	•3770- •3846-	.0102 .0100	•0258 •0134	•17∠8 •1466
	133	797	90.00	10.00-	65.10	90.22	10.00-	1.3877	•0219- •0345-	• 4224-	.0100	•0154	1219
	133	798	90.00		108.50			1.3462	.0414-	4753-	•0056	•0092-	-1380
	134	799	•00	15.CO-	15.60	.00	.00	.0056-	-0084	.0062-		.0056	.0132-
	134	BUL	.00	15.60-	20.00	•00	.00	.0088	•0071	.0099-	.0000	.0042	-0100-
200	134	B01	•00	15.00-	30.00	.00	•00	.0031-	•0077	.0002-	.0000	.0024	-0068-
		B∪2	.00	15.66-	40.00	.00	•00	.0026-	-0080	.0020	.0002	.0019	•0054-
200	134												
200 200	134 134 134	803 804	.00	15.60-	60.00 100.00	.00	•00	.0017- .0010-	.0077 .0076	.0040 .0044	.0001	.0006 .0009	.0012- .0010-

 $^{^{\}dagger}\mathbf{Minus}$ signs are to the right of the numbers to which they apply.

TABLE III. - AERODYNAMIC COEFFICIENTS OF MODEL FOR THE COMPLETE INVESTIGATION - Continued

Config.	Run	Point	α ₁ , deg	ø, deg	q, lb/sqft	α, deg	β, deg	C _N	C _A	C _m	C ₁	C _n	CY
200	135	805	10.00	15.00-	15.00	9.67	2.58-	.1163	.0067 .0076	.0524	.0024	.0207 .0132	.0166- .0006
200	135	8.26	10.00	15.00 15.00-	20.00 30.00	9.67 9.67	2.58-	.1394 .1284	1 .0080	.0558	.0017	-0147	.0005
200	135 135	807 808	10.00 10.00	15.00-	40.00	9.68	2.58-	.1161	.0079	.0570	.0017	-0142	•0012
	135	809	10.00	15.00-	60.00	9.68	2.58-	.1127	•0076	.0622	.0015	•0135	•0039
	135	810	10.00	15.60-	100.00	9.70	2.59-	.1172	.0073	.0590	.0016	•0121	•0065
200	136	811	20.00	15.00-	15.00	19.39	5.08-	.4366	-0021-	.0317-	.0039	.0338 .0315	•0264 •0371
200	136	812	20.00	15.60-	20.00	19.40	5.08-	.4340	.0017-	.0306+ .0181-	.0042	.0280	.0439
	136	813	20.00 20.00	15.00- 15.00-	30.00 40.00	19.41	5.09- 5.09-	3718	-0014-	.0005-	.0033	.0275	+0465
20C 20C	136 136	814 815	20.00	15.00-	60.00	19.45	5.09-	.3776	.0025-	.0076	.0031	-0268	•0562
200	136	816	20.00	15.00-	100.00	19.50	5.11-	.3723	.0022-	•0175	.0036	•0339	•0290
200	137	817	30.00	15.00-	15.16	29.15	7.43-	.0870	.0073-	.3465	-0128	+1247	-1629-
200	137	818	30.00	15.00-	20.21	29.22	7.45-	•9205	.0131-	•1650- •1747-	.0120 .0129	•1175 •1293	•1386- •1807-
200	137	819	30.00	15.00-	30.32 40.42	29.44	7•45- 7•46-	.8314 .8457	.0049- .0070-	1863-	.0141	1389	1969-
200 . 200	137	820 821	30.0U 30.0U	15.00- 15.00-	60.64	29.33	7.47-	.8505	-0124-	.1824-	.0144	+1401	-1723-
200	137	822	30.00	15.00-	101.06	29.44	7.50-	-8417	-0155-	.1620-	.0115	•1413	.0684-
200	138	823	40.60	15.00-	15.34	39.09	9.59-	1.3665	.0386-	.0922-	.0178	-1455	-0807-
200	138	824	46.00	15.00-	20.45	39.13	9.60-	1.4925	-0321-	.2287-	.0240	•1825	•3043- •3563-
200	138	825	40.00	15.00-	30.68	39.16	9.60-	1.2529	.0276- .0328-	•1692- •2314-	.0242 .0245	.0716 .0879	.3506-
200	.138	826	40.00 40.00	15.00-	40.90 61.35	39.21	9.61- 9.63-	1.2839	.0334-	-2598-	.0247	.1026	.3389-
200 200	138 138	827 828	40.00	15.00-	102.25	39.51	9.67-	1.3289	.0343-	+2278-	.0263	•0966	•3069-
200.	139	829	50.00	15+00-	15.57	49.11	11.45-	1.6207	.0513-	.0398	.0211	.1625	.1179
200.	139	830	50.00	15.60-	20.76	49.14		1.6356	.0544-	.0101-	.0207	-1181	.1395
200	139	831	50.00	15.00-	31.15	49.19		1.4996	•0602-	-1415-	.0205 .0211	.0860 .0817	.0308 .0054
200	139	832	50.00	15.60-	41.53	49.45	11.47- 11.49-	1.5299	.0631- .0592-	.2300- .2469-	.0214	.0421	.0233-
200 200	139 139	833	50.00 50.00	15.60- 15.60-	62.29 103.82	49.36	11.53-	1.5117	.0621-	.1857-	.0217	-0262	.0439-
	140	835	60.00	15.00-	15.83	59.22	12.96-	1.5861	.0789-	.0342	.0142	-2658	.4782
200	140	836	60.00	15.00-	21.10	59.25		1.5650	-0840-	.0274-	.0137	•2683	5023
200	140	837	60.00	15.40-	31-65	59.29	12.97-	1.4152	-0867-	.0495- .0896-	.0153	•2657 •2104	•4654 •3663
200	140	838	60.00	15.00-	42.20	59.34 59.47	12.98-	1.4357	•0854- •0874-	.1138-	.0148 .0145	1088	-2111
200	140	839 840	60.00 60.00	15.00- 15.00-	63.30 105.50	59.67	13.02-	1.4104	.0864-	.0926-	.0131	•0433	•1141
			76.00	15.00-	16.13	69.44	14.08-	1.4748	.0745-	.0309	.0123	.1999	.3980
200 200	141	841 842	70.00 70.00	19.00-	21.50	69.46	14.09-	1.4214	•0772-	.0664-	.0129	-2671	-5011
200	141	843	70.00	15.00-	32.25	69.50		1.3203	•0708-	-1191-	.0132 .0117	•2634 •1727	•4949 •3939
200	141	844	70.00	15.00-	43.00	69.56	14.09-	1.3277	.0785- .0917-	•1483- •1504-	.0135	1041	-3034
200	141 141	845 846	70.00	15.00-	107-50	69.67 69.90		1.3708	.0906-	•1565-	.0137	•0484	.2226
	l				14 33	79.74	14.77-	1.3931	./0484−	•0952	.0120	-0749	.2712
200	142	847 848	80.00 80.00	15.00- 15.00-	16.22			1.4539	.0650-	.0551-	.0123	•0904	.3044
200	142	849	80.60	15.00-	32.43	79.82	14.77-	1.3547	.0540-	.1317-	•0125	•0608	•2598
200	142	850	80.00	15.00-	43.24	79.88	14.78-	1.3840	.0635- .0692-	•1720- •2146-	.0132 .0134	.0118 .0179	.2076 .2096
200	142	851 852	80.00	15.60- 15.60-	108-10		14.78-	1.3283	.0759-	.2489-	.0135	•0175	.1827
i		i				l	15.00-	1.3982	.0010-	.3703-	.0107	.0544	.2887
200 200	143	853 854	90.GU 90.GU	15.00- 15.00-	16.28 21.70			1.3568	.0017-	.3747-	.0121	•0717	•3049
200	143	855	90.00	15.00-	32.55	90.15	15.00-	1.2957	•0103-	•3744-	•0121	•0791	•3187 •2752
200	143	856	90.00	15.00-	43.40	90.21	15.00-	1.3022	.0243- .0349-	•3816- •4083-	.0131 .0133	•0368 •0068	-2458
200	143	857	90.00	15.00- 15.00-	65.10 108.56		15.00-	1.2965	.0454-			•0177-	-2078
		l	1	• • • • •	15.00	.00	.00	.0821	.0057	.0496-	.0000	.0030	-0022-
200	144	859 860	.0u	20.60-	15.00	.00	.00	.0616	.0069	•V372~	.0000	.0023	•0016-
200	144	861	1 .00	20.00-	30.00	.00	•00	.0323	.0064	+0186-	.0000	•0015	•0013-
200	144	862	•00	20.00-	40.00	•00	•00	.0177	.0072	.0052- .0060-	.0000	.0017	.0016-
200	144	863 864	.00	20.00- 20.00-	100.00	00	.00 .00	.0163 .0097	.0070	.0011-		.0006	.0007
	1			l	ì	9.41	3.41-	.1713	.0051	.0191	.0023	.0191	.0056
200	145 145	865 866	10.00	20.00-	15.00	9.41	3.41-	.1713	.0018	.0762-	.0023	•0156	+0177
200	145	867	10.00	20.00-	30.00	9.41	3.41-	.1311	.0064	.0435	•0017	•0180	•0062
200	145	868	10.00	20.00-	40.00	9.42	3.417	.1247 .1188	.0064 .0067	.0503 .0547	.0019	•0166 •0165	.0087
200	145 145	869 870	10.00	20.00- 20.00-	100.00	9.42	3.41-	.1139	.0069	.0575	.0020	-0164	•0091
			1		15.00	18.90	1	.4471	.0045-	.0481-	.0030	.0502	.0354
200	146	871 872	20.00	20.00-	20.00	18.91	6.72-	.4424	.0035-	-0554-	.0044	•0465	.0443
200	146	873	20.00	20.00-	30.00	18.92	673-	.3952	.0014-	.0322-		-0416	0533
200	146	874	20.00	20.00-	40.00	18.93	6.73-	.3908	.0014-	.0262- .0182-	.0049	.0440 .0432	.0451 .0451
200	146	875	20.00	20.00-	100.00	18.96	6.74-	.3827 .3782	.0009-	.0071-	.0049	.0437	.0444
		876	120.00	2000-	1 700 800	1	1 32.75	1	1	1	1	1	1

 $[\]dagger_{\mbox{Minus signs}}$ are to the right of the numbers to which they apply.

TABLE III. - AERODYNAMIC COEFFICIENTS OF MODEL FOR THE COMPLETE INVESTIGATION - Continued

Config.	Run	Point	α1,	ø,	q, lb/sqft	a, deg	β, deg	C _N	C _A	C _m	c,	Cn	С¥
			deg	deg									1101
200	147 147	877 878	36.00 36.00	20.00-	15.16 20.21	28.53 28.54	9 • 86 - 9 • 86 -	.9375 .9193	.0114- .0123-	•1916- •2101-	.0138 .0121	•1267 •1271	•1193- •0981-
200	147	879	30.00	20.00-	30.32	28.57	9.87-	.8212	.0119-	.2006-	.0129	•1383	.1137-
200	147	880	30.00	20.60-	40.42	28.60	9+86-	.8178	.0082-	.2285-	•0151	•1649	•1696-
200	147	881 882	30.00 30.00	20.00-	101.06	28.66 28.76	9•90- 9•93-	.8571 .8372	.0058- .0115-	•2327- •2000-	.0171 .0140	•1751 •1645	•1641- •0539-
200	147	862	30.00	20.00-	101.08	20.70	7.75-	•0512	.0113-	•2000	.0140		•0337
200	148	883	40.00	20.00-	15.34	38.33	12.72-	1.4497	•0295-	.2264-	•0236	•1887	+2095-
200	148	884 885	40.00	20.00-	20.45 30.68	38.35 38.39	12.72-	1.4589	.0262- .0279-	•2752- •1987-	.0253 .0274	•1819 •0765	•2763~ •3375~
200	148	886	46.00	20.00-	40.90	38.43	12.75-	1.2399	.0277-	•2151-	.0249	•0473	•3066-
200	148	887	40.00	20.00-	61.35	38.51	12.77-	1.2170	.0290-	.2590-	.0258	•1001	•2689~
200	148	888	40.00	20.00-	102.25	38.70	12.82-	1.3015	•0322-	•2476-	•0288	1260	•2257-
200	149	889	50.00	20.00-	15.57	48.32	15.21-	1.6682	.0499-	.0782-	.0243	.0571	•1917
200	149	890	50.00	20.00-	20.76	48.34	15.21-	1.5894	-0458-	.0994-	.0220	•0426	•2055
200	149	891	50.00	20.00-	31.15	48.40	15.23-	1.5701	+0467- +0487-	•1681- •2291-	.0227 .0232	.0114- .0036-	•1283 •1317
200	149	892 893	50.00 50.00	20.00-	41.53 62.29	48.45 48.58	15.24- 15.27-	1.5385	.0490-	.2547-	•0235	•0259-	•1043
200	149	894	50.00	20.00-	103.82	48.78	15.31-	1.4892	.0496-	-2380-	.0223	.0252-	•1185
										0000	0177	V 0 0 0	6400
200	150 150	895 896	60.00 60.00	20.00-	15.83 21.10	58+51 58+54	17-24- 17-25-	1.4675	•0767- •0747-	•0322- •0676-	-0177 -0174	•3090 •2724	•5493 •5106
200	150	897	60.00	20.66-	31.65	58.59	17.26-	1.4053	.0783-	.0911-	•0182	.2431	.4724
200	.150	898	60.00	20.00-	42.20	58.64	17.27-	1.3725	-0753-	.1235-	.0173	•2021	•4247
200	150	899	60.Cu	20.00-	63.30	58.75	17-29- 17-32-	1.4248	•0772- •0786-	.1290~	.0188	•0807 •0396	•2474 •1857
200	150	900	60.00	20.00-	105.50	58.96	1,,,,,,	100943	•0100	.1169-	-0185	.0370	****
200	151	901	70.00	20.00-	16.13	68.92	18.76-	1.5239	.0794-	.0161	.0172	•2255	•4770
200	151	902	70.00	20.00-	21.50	68.94	18.76-	1.4161	-0789-	.0788-	•0167	+2526	•5321
200	151 151	903 904	70.00 70.00	20.00- 20.60-	32.25 43.00	68.98 69.01	18.77- 18.77-	1.3255	.0839- .0837-	•1811- •1915-	.0185 .0179	•2869 •2421	.6041 .5489
200	151	905	70.00	20.60-	64.50	69.14	18.79-	1.3163	0853-	.1934-	.0184	•1508	4189
200	151	906	70.00	20.60-	107.50	69.34	18.81-	1.2985	-0885-	•1953-	.0183	•1000	•3575
200	152	907	80.00	20.00-	16.22	79.46	19.69-	1.4936	•0625-	.0680~	•0176	•0954	+3621
200	152	908	80.00	20.00-	21.62	79.49	19.69-	1.4614	•0654-	•U857-	.0175	•0953	•3753
200	152	909	80.00	20.00-	32.43	79.54	19.69- 19.70-	1.3498	•0605- •0596-	•1664-	.0186	•1104 •0823	•3949 •3694
200 200	152	910 911	80.00 80.00	20.00-	43.24 64.86	79.59 79.68	19.70-	1.3152	.0682-	•2130-	.0183	•0271	.2862
200	152	912	80.00	20.60-	108.10	79.88	19.71-	1.2591	.0671-	-2567-	.0186	•0171	.2571
						00.00	20.00-	1.4320	.0023	.3771-	.0179	•0538	.3610
200 200	153 153	913 914	90.00	20.00-	16.28 21.70	90.12	20.00-	1.4115	.0023	3031-	.0176	.0581	.3738
200	153	915	90.00	20.00-	32.55	90.16	20.00-	1.3078	•0085-	.4123-	.0184	•0858	•4267
200	153	916	90.00	20.00-	43.40	90.20	20.00-	1.2638	.0172-	.4222-	.0179	•0770	-4137
200 200	153 153	917 918	90.00	20.60- 20.60-	65.10 108.50	90.30	20.00-	1.2524	.0309-	.4031- .4268-	.0184 .0175	•0329 •0311-	•3360 •2349
200	133	710	70.00	20.00	100.50	,,,,,,	1:000	102041	*****		į		1
200	154	919	-00	30.00-	15.00	.00	.00	.0045-	•666	.0014	.0001	•∪057 •∪043	•6137-
200 200	154 154	920 921	.0u	30.00-	30.00	•00 •00	.00	.0034- .0019-	.0076 .0080	.0031	.0001	.0020	.0019-
200	154	922	.00	30.00-	40.00	.00	.00	.0017-	.0083	.0056	.0000	.0012	-0016-
200	154	923	•0∪	30.00-	60.00	.00	•00	•0013-	.0085	.0072	.0002	•0012	-0015-
200	154	924	.00	30.60-	100.00	•00	•00	.0008-	-0077	.0059	.0001	•0009	-0011-
200	155	925	10.00	30.00-	15.00	8.68	4.98-	.0889	.0079	.0652	.0030	.0261	•0133
200	155	926	10.00	30.00-	20.00	8.69	4 98-	.0938	.0102	.0681	.0027	•0265	•0058
200	155 155	927 928	10.00	30.00- 30.00-	30.00 40.00	8.69 8.69	4.98-	.0908	.0094 .0085	.0661 .0641	.0024	•0245 •0224	.0096
200	155	929	10.00	30.00-	60.00	8.69	4.99-	0914	.0078	-0639	.0029	-0218	.0183
200	155	930	10.00	30.60-	100.00	8.70	4.99-	.0910	.0009-	.0643	.0028	•0223	.0159
200	156	931	20.00	30.00-	15.00	17.51	9.85-	.3670	.0053	.0252-	•0076	.0748	.0318
200	156	932	20.00	30.00-	20.00	17.51	9.85-	.3447	.0042	.0212-	.0074	.0641	.0495
200	156	933	20.00	30.00-	30.00	17.52	9.86-	.3258	.0041	.0150-	.0060	+0641	•0457
200	156	934	20.00	30.00-	60.00	17.53	9.86-	-3144	.0034	•0101-	•0075	-0667	.0426 .0372
200	156 156	935 936	20.00	30.00- 30.00-	100.00	17.58	9•87- 9•89-	•3255 •3270	.0041 .0031	.0155- .0120-		+0695 +0698	.0406
				1			i						1
200	157	937	30.00	30.00-	15.16		14.49-	•7437 •7466	.0015 .0000	•1552- •1741-	.0184 .0201	•1648 •1691	•0207- •0423-
200	157 157	938 939	30.00 .		20.21 30.32			.7238	0000	.1921-	.0216	•1762	.0734-
200	157	940	30.00	30.00-	40.42	26.65	14.52~	.7196	.0003	-2187-	.0209	.1832	.0650-
200	157	941	30.00	30.00-	60.64		14.54-	•7279	.0004-	•2297-		•2005 •1871	-0479-
200	157	942	30.00	30.00-	101.06	26.79	14.58-	•7311	•0036-	.2076-	.0200	•19/1	•0026-
200	158	943	40.00	30.00-	15.34		18.77-		.0179-	•1769-		•1286	•1196-
200	158	944	40.00	30.00-			18.78-	1.2490	•0176~	•1610-		-0986	.0882-
200	158	945 946	40.00 40.00	30.00- 30.00-	30.68 40.90	36.11 36.14	18.80- 18.81-		.0197- .0208-	.1788- .2090-	.0340	+0834 +0869	.1523~ .1662-
200			. ************************************	3 3 0 0 0 0 0 -	40.00		10.01-	101-10					
200	158 158	947	40.00	30.00-	61.35	36+22	18-84-	1.1714	•U256-	-3001-	.0350	•1621	-1163-

 $^{{}^{\}dagger}\text{Minus signs}$ are to the right of the numbers to which they apply.

TABLE III. - AERODYNAMIC COEFFICIENTS OF MODEL FOR THE COMPLETE INVESTIGATION - Continued

Config.	Run	Point	α ₁ , deg	ø, deg	q, lb/sq ft	α, deg	β, deg	C _N	C _A	C _m	c,	Cn	С¥
200	159	949	50.00	30.00-	15.57	45.97	22.55-	1.4228	.0340-	.0037	.0295	•0416 •0010	•3036 •2467
200	159 159	950 951	50.00	30.60- 30.60-	20.76	45.99	22.55-	1.3583	.0319- .0353-	.0091 .0109	.0290	.0010	.1251
200	159	952	50.00	30.00-	41.53	46.08	22.59-	1.3571	0349-	.0403-	.0300	.0252-	-1047
200	159	953	50.00	30.00-	62.29	46.18	22.62-	1.3852	.0424-	•1961-	.0275	•UZQ4-	.2516
260	159	954	50.00	30.66-	103.82	46.36	22.68-	1.3542	.0497-	.1706-	•0273	•∪286	.2759
200	160	955	66.00	30.00-	15.83	56.37	25.68-	1.2468	.0611-	.0089	.0255	-2924	.7097
200	160	956	60.00	30.00-	21.10	56.40	25.68-	1.1369	.0539-	.0233-	.0250	·2536	.6063 .5420
200	160	957 958	60.00	30.00- 30.00-	31.65	56.44	25.69- 25.71-	1.1618	.0551- .0553-	.0530- .0820-	.0253	•1314	.4489
200 200	160	959	60.00	30.00-	63.30	56.57	25.73-	1.1921	-0536-	.0709-	.0277	.0693	-2847
200	160	960	60.00	30.60-	105.50	56.75	25.77-	1.2160	.0581-	-8650.	.0274	•0684	•3834
200	161	961	70.60	30.00-	16.13	67.27	28.04-	1.1835	•6662-	•0304	.0236	.2154	.6227
200	161	962	70.00	30.00-	21.50	67.28	28.04-	1.0656	.0646-	• J8 48 -	-0240	• 2447	.6606
200	161	963	70.00	30.00-	32.25	67.32	28.05-	1.0293	.0713-	•1707-	•0254	•2547	•6806
200	162	967	80.00	30.00-	16.22	78.56	29.51-	1.2021	.0543-	·C125-	.0254	•1191	اددد.
200	162	968	80.00	30.00-	21.62	78.59	29.51-	1.1418	•U577-	.0530-	.0257	-1411	•>601
200	162	969	80.00	30.00-	32.43	78.62	29.51-	1.0198	•0533-	-1480-	.0250	45 د 1 •	•>>71
200	162	970 971	80.00 80.00	30.00- 30.00-	43.24 64.86	78.66 78.76	29•52- 29•52-	1.0284	.0525- .0647-	•2017- •1802-	.0254 .0280	•1281 •0592	•2602 •4470
200 200	162 162	972	80.00	30.00-	108-10	78.93	29.54-	1.0997	.0686-	.2181~	.0277	76 د ن	-4024
	•	1							(14.7	2070	0.757	0,43	
200	163 163	973 974	90.00	30.00- 30.00-	16.28 21.70	90.07	30.00-	1.1199	.0142 .0166	•2978- •2998-	.0257 .0251	•0442 •0452	•4864 •4867
200	163	975	90.00	30.60-	32.55	90.13	30.00-	1.0550	.0109	.3492-	.0260	0550	.4766
200	163	976	90.60	30.00-	43.40	90.17	30.00-	1.0626	•0003	.4618-	.0275	.0632	.4668
200	163	977	90.00	30.00-	65.10	90.25	30.00-	1.0567	.0203~	•3609-	.0280	•0011	-3849
200	163	978	90.00	30.66-	108.50	90.41	36.00-	1.0388	•0299-	•3679-	•0274	•0121-	.3654
200	164	979	60.00	5.00	15.83	60.00	4.33	1.7732	-0680-	.1444	.0063-	•1991-	•328B-
200	164	980	60.00	5.00	21.10	60.03	4.33	1.7175	•0777-	.0256	•0047-	-1574-	-2470-
200 206	164	981 982	60.00	5.00 5.00	31.65	60.09 66.13	4.33	1.6079	.0869- .0875-	•1034- •1308-	.0035- .0024-	.0869- .0297-	-1228- -0295-
200	164 164	983	60.00	5.60	63.30	60.26	4.34	1.5434	.0961-	.1476-	.0025-	.0171	.0250
200	164	984	66.00	5.60	105.50	60.50	4 • 3 5	1.5529	•6950-	-1241-	.0024-	·C244	• C3 C3
200		985	70.00	5.00	16.13	70.63	4.70	1.6028	.650-	•026∠	.0027-	.0695	.0203
200	165 165	986	70.00	5.00	21.50	70.06	4.70	1.6832	.0771-	.0044-	.0032-	1156	8880
200	165	987	70.00	5.00	32.25	70.12	4.70	1.5563	.0785~	-0920-	•0043-	•1075	■ DB14
200	165	988	70.00	5.00	43.00	70.17	4.70	1.5179	•C828-	•1406-	.0043-	•0807	.0354
200 200	165 165	989 990	76.00	5.60 5.60	64.50 107.50	70.30	4.71	1.5514	•0879- •0864-	•1751- •1805-	.0038-	.0572 .0404	.08G
200	105	330	1,0.00	3.00	10,4,50	10.52	1	104030	1 1			•	
200	166	991 992	80.00 80.00	5.00 5.00	16.22	80.07	4.92	1.5904	•0606- •0598-	•0280- •0644-	.0037-	•0216- •0142	•1012- •0722-
200	166 166	993	80.00	5.00	32.43	80.15	4.92	1.5636	.0632-	-1643-	.0041-	-0079	-0596-
200	166	994	80.00	5.00	43.24	80.20	4.92	1.4550	-0591−	•2147-	-8600.	•3066	•U606-
206	166	995	80.00	5.00	64.86	80.32	4.93	1.4517	•6719- •6740-	•2791- •2903-	.0043-	.0013- .0109	-0608- -0366-
200	166	996	80.00	5.00	108.10	80.53	4.93	1.4000	•0,40-	•2,05	••••	*****	l.
200	167	997	90.00	5.00	16.28	90.10	5.00	1.6223	.0021-	•4167-	.0024-	.0336- .0214-	.0817-
200	167	998 999	90.00	5.60 5.60	21.70 32.55	90.13	5.00 5.00	1.5902 1.4893	.0061- .0146-	•4123- •4148-	.0035-	.0302-	.0671-
200	167 167	1000	90.00	5.00	43.40	90.23	5.60	1.4391	0253-	.4162~	.0043-	.0325-	.0700-
200	167	1001	90.00	5.60	65.10	90.35	5.00	1.4643	.0387-	•4766-	.0041-	•0021	•0z48~
200	167	1002	90.00	5.00	108.50	90.56	5.00	1.3943	-0451-	-7د050	-8د00٠	•0146	•6613-
200	168	1003	60.00	10.00	15.83	59.72	8.65	1.7073	.0686-	.0914	•0121-	.2499-	-7د46.
260	168	1004	66.00	10.00	21.10	59.74	8.66	1.6201	.0713-	.0058-	.0104-	•2097-	+3946-
200	168	1005	60.00	10.60	31.65	59.80	8 • 6 6	1.5280	•0772-	.6541-	•0097-	•1397-	+2728-
200	168	1006	60.00	10.00	42.20	59.85 59.97	8 • 6 7 8 • 6 8	1.5202	.0839- .0988-	•1109- •1137-	.0094- .0085-	•0876~ •0131	•1746-
200	168 168	1607	60.00	10.00 10.00	63.30 105.50	60.21	8.70	1.5289	.0956-	.1390-	.0078-	.0355-	.0411-
					1				04.05	0.500	2004	.1835-	.3906-
200	169 169	1009	70.00	10.00 10.00	16.13 21.50	69.82	9.39	1.6164	.0685- .0691-	.0230 .0593-	.0094-	-2082-	.4246-
200		1011	70.00	10.60	32.25	69.90	9.40	1.5098	.0779-	-1666-	.0095-	-0852−	•2619-
206	169	1012	70.60	10.00	43.00	69.96	9.40	1.5099	.6797-	.1621-	.0091-	•C532	•0861-
200		1013	70.00	10.00	64.50 107.50	70.07	9.41	1.4794	.0877~ .0947-	•1742- •1704-	•0077- •0079-	.0414- .0486-	.1746- .1562-
200	169	1014	70.00	10.00	107.50	70.31		1.0130	l i			İ	
200	170	1015	80.00	10.60	16.22	79.95	9.85	1.5360	• U550-	. 478-	.0074-	-4440	• 2148-
200		1016	80.00	10.00	21.62	79.98	9 - 85	1.5109	•0583- •0601-	.0579− .1519−	.0078-	•0287- •0046	•1745- •1329•
200		1617 1618	80.00	10.00	32.43	80.03 80.09	9.65	1.4725	.0565-	.2116-	-0090-	•0188-	•1603-
200		1019	80.00	10.00	64.86	80.20	9.85	1.4167	.629-	.2530-	.0095-	·CU69-	-1321-
200		1026	86.60	10.00	108.10	80.46	9.86	1.3799	•0633-	•2663-	.0089-	.0120	•1136-
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 $^{^{\}dagger}$ Minus signs are to the right of the numbers to which they apply.

TABLE III. - AERODYNAMIC COEFFICIENTS OF MODEL FOR THE COMPLETE INVESTIGATION - Continued

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Config.	Run	Point	α ₁ , deg	ø, deg	lb/sq ft	α, deg	β, deg	c _N	C _A	C _m	c,	Cn	CY
200	171 171	1021	90.00 90.00	10.60	16.28 21.70	90.09 90.12	10.00	1.5440	.0003-	•3855- •3718-	.0071-	+6433- +6464-	•1910- •1695-
200	171	1623	90.00	10.00	32.55	90.17	10.00	1.4333	0173-	-3899-	.0081-	.0443-	1654-
200	171	1024	90.00	10.CO	43.40	90.23	10.00	1.4227	-6231-	•4212-	.0084-	•0499-	-1654-
200 200		1025	90.00	10.00	65.10 108.50	90.33	10.00	1.3960	.0383- .0448-	•4134- •4745-	.0088-	.0143- .0161	.1198- .0781-
200	l	1027	60.00	15.60	15.83		12.96	1.6684	.0584-	•0541	.0149-	-2957-	-5085-
200	172	1028	60.00	15.00	21.10	59.25	12.97	1.5368	+0604-	•0172	.0139-	•2562-	.4283-
200 206		1029	60.00	15.00 15.00	31.65 42.20	59.30 59.37	12.97	1.5192	+0731- +0780-	•0154-	.0129-	•1552-	•3015-
200		1030	60.00	15.00	63.30		13.00	1.5119	.0780-	•0581~ •1265~	.0127-	•0671- •0071	.1605- .0093-
200		1032	60.00	15.00	105.50		13.02	1.4178	- 0864-	.1034-	.0103-	.0281-	.0775-
200 200		1033 1034	70.60 70.00	15.00 15.00	16.13 21.50	69.44 69.46	14.08	1.5850	.0618-	.0029 .0137	.0132-	•2233- •1782-	.4085- .3672-
			1				1		1	i		l	
200 200	174	1039	80.00	15.00 15.00	16.22	79.75 79.77	14.77	1.5217	.0506-	.0522- .0443-	.0117-	•0770- •0632-	.2448- .2581-
200	174	1041	80.00	15.00	32.43	79.84	14.77	1.4256	.0475-	1589-	.0126-	.0487-	•2240-
200	174	1042	80.00	15.00	43.24	79.89	14.78	1.4100	.0572-	-1992-	.0125-	.0427-	-2084-
200	174	1043	80.00	15.00	64.86	79.98	14.78	1.3475	•0593-	.2334-	-0128-	•0219-	•1793-
200	174	1044	80.00	15.00	108.10	80.21	14.79	1.3616	-0651-	•2513-	-0124-	•0045	•1442-
200	175	1045	96.00	15.60	16.28	90.08	15.00	1.4518	+0067	-3514-	-0115-	.0631-	-2516-
200		1046	90.00	15.00 15.00	21.70 32.55	90.11	15.00 15.00	1.4249	•0006	•3672-	.0120-	•0819÷	-2640-
200	175	1047	90.00	15.00	43.40	90.15	15.00	1.4164	.0129-	•3806- •3888-	.0125-	•0663- •0597-	•2499- •2447-
200		1049	90.00	15.00	65.10	90.33	15.00	1.3569	.0360-	.4106-	.0127-	-0404-	2078-
200	175	1050	96.00	15.00	108.50	90.54	15.00	1.3331	.0465-	.4181-	0122-	.0110	-1509-
300	87	518	.00	.00	15.00	.00	•00	.0209	.0428	.0109	.0006-	.0000	.0042
300	87	519	•0u	•00	20.00		• • • •	.0104-	.0417	.0247	.0000	•0016	.0024
300 300	87 87	520 521	.cu	•00	30.00 40.00	•00	•00 •00	.0192 .0147	.0420	.0019 .0039	.0000	•0016	•0011
300	87	522	.00		60.00	.00	•00	.0182	.0422	.0005-	.0000	•0018	.0006
300	87	523	.00	•60	100.00	•01	•00	•C158	.0433	.0010	.0002	-0004-	•0032
300	88	524	5.00	•00	15.00	5.01	•60	•2776	.0355	.0325	.0005-	-0042-	.0228
300	88 88	525	5.00 5.00	•60	20.00	5.01	•00	•3112	■0351	.0072 .0114	.0004-	•0002	.0063
300 300	88	526 527	5.00	•00	30.00 40.00	5.03 5.03	•U0	.2923 .2835	.0355	.0114	.0002	•000C	.0050 .0059
300	88	528	5.00	.00	60.00	5.06	•00	.3046	.0346	.0029	.0005	+0002	.0039 60000
300	88	529	5.00	.00	100.00	5.11	•10	.3055	.0341	.0033	.0005	-0006-	.0043
300	89	530	10.00	.60	15.00	10.02	•00	.5856	.0276	.0687	.0002-	.0006-	•0116
300 300	89 89	531 532	10.00	•00	20.00 30.00	10.03	•00	•5932 •5927	.0273 .0266	.0016 .0079-	•0003-	.0013-	•0098
300	89	533	10.00	•00	40.00	10.08	•00	.6050	.0275	.0079-	.0004	.0005 .0002-	7 د00 • 0042 •
300	89	534	10.00	.00	60.00	10.12	•30	5948	0275	.0026-	.0005	.0002-	•0042 •0016
300	89	535	10.00	.00	100.00	10.22	•00	.6122	.0280	.0058-	.0005	•0012-	د0045
300	90	536	15.00	.00	15.00	15.04	•00	.8254	.0252	•0037-	.0004-	•6024	د ٥٥١٠
300	90	537 538	15.0L	 	20.00 30.00	15.06 15.09	•00	.8897 .8498	.0271 .0266	.0364- .0245-	.0002	.0013	+0002
300	93	539	15.00	.00	40.00	15.11	•00	8298	.0260	.0185-	.0002	•0002 •0007	.0045
300	90	540	15.00	.00	60.00	15.19	•00	.8521	.0253	.0209-	.0003-	.0000	.00∠8
300	90	541	15.00	•60	100.00	15.32	.00	.8611	• J249	.0192-	.0004-	.0013-	•0060
300	91	542	20.00	•00	15.00	20.06	• U G	1.1349	-0180	.0279-	.0004-	•0022-	•0217
300	91	543 544	20.00 20.00	•00	20.00 30.00	20.08	• 00	1.1227	•0191	•0611-	.0004-	•0004	.0081
300	91	545	20.00	•00	40.00	20.16		1.0746 1.1012	•J187 •J178	.0446- .0514-	.0009-	.0016 .0012	•0071 •0059
300	91	546	20.00	.00	60.00	20.25		1.1182	5172	.0504-	.0006-	.0017	-0042
300	91	547	20.00	•00	100.00	20.42		1.1421	•3168	.0507-	.0012-	.0001	.0046
300	92	548	25.00	•60	15.00			1.4456	• 3090	.0663-	.0001	•0032	•011C
300	92	549	25.00	•00	20.00			1.3809	- 3081		.0003	.0022	•0150
300	92	550 551	25.00 25.00	.00	30.00 40.00	25.20	•00 •00	1.3484	.J078 .J074	•0805- •0866-	.0030- .0048-	.0054 .0032	.0066
300	92	552	25.00	•60	60.00	25.30	•00	1.3693	-3074	-0994-	*00T8-	-0032	.000c
30L	92	553	25.00	•60	100.00			1.3921	. 7058	-1881-	.0000	.0002	·0123
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 $^{^{\}dagger}$ Minus signs are to the right of the numbers to which they apply.

TABLE III. - AERODYNAMIC COEFFICIENTS OF MODEL FOR THE COMPLETE INVESTIGATION - Continued †

Config.	Run	Point	α ₁ , deg	ø, deg	q, lb/sq ft	α, deg	β, deg	c _N	C _A	С т	c,	Cn	CY
300	93	554	30.00	•60	15.16	30.10	•00	1.8039	•0115-	•0336-		•0017	.0132
300 300	93	555 556	30.00 30.00	.00	20.21 30.32	30.13 30.18	•up	1.7100	-0060- -0058-	•1043- •1147~	.0004	.0017 .0046	.0239 .0140
300	93	557	30.00	1	40.42	30.23	•00	1.5565	.0081-	1324-	.0044-	.0002-	.0013-
300	93	558	30.00	-00	60.64	3,0.35	•00	1.5683	-0075-	•1414-	.0033-	•0053	• 0034
300	93	559	30.00	•00	101.06	30.61	•00	1.6354	•0087-	-1382-	•0003	•0009	•0117
300	94	560	35.00	•00	15.16	35.11	•00	2.1098	-0300-	.0035-	.0107-	.0111	.0621-
300 300	94	561 562	35.00 35.00	.00	20.21 30.32	35.15 35.20	•00	2+0643 1+8930	.0241-	.0532- .1375-	.0026-	•0061 •0007	.0469-
300	94	563	35.00	.00	40.42	35.26	•00	1.7980	.0220-	1686-	.0019	.0045-	.0247-
300	94	564	35.00	ن ن•	60.64	35.40	•60	1.8298	.0242-	-1929-	.0029	-0065-	-0032-
300	94	565	35.00	•00	101.06	35.69	•00	1.8656	.0047-	•1872-	.0037	•0040-	•0013
300	95	566	40.00	•00	15.34	40.15	•00	2.5870	.0460-	.0430-	•0277-	-0348	-2765-
300 300	95 95	567 568	40.00	.00	20.45	40.18	•00	2.3366	.0462-	.0617-	.0135~	.0026~ .0102-	•1819- •0140-
300	95	569	40.00	.00	30.68 40.90	40.24	.00	2.0000	.0372-	.1469- .2153-	.0060	•0102-	-0160-
300	95	570	40.00	.00	61.35	40.42	•00	1.8560	.0396-	.1849-	.0031	.0074-	-0015
300	95	571	40.00		102.25	40.74	.00	1.9581	.0443-	.2180-	•0075-	+0268	+0247
300	96	572	45.00	•00	15.34	45.14	.00	2.4525	.0316-	.0604-	-0186-	•0743-	•2∠50~
300 306	96 96		45.00 45.00	•00	20.45 30.68	45.18 45.25	•00 •00	2.3901	•0527- •0475-	•0533- •1632-	.0024-	•0347- •6318-	•2282- •0299-
300	96		45.00	.00	40.90	45.33	•00	2.1479	.0523-	•2439-	.0068	.0109-	-0059-
300	96	576	45.00	•00	61.35	45.49	•00	2.1419	.0537-	.3034-	0001	•0139	.0207
300	96	577	45.00	•00	102.25	45.79	• • •	2.0920	.0505-	•2736-	•0025-	•0508	•0452
300	97	578	50.06	•00	15.57	50.13	•00	2.2908	-0332-	•0590-		•1524-	-2538-
300	97 97	579 580	50.00 50.00	•00	20.76	50.18 50.25	•00	2.3224	•0404- •0458-	•0669- •2014-	.0009-	•1053- •0596-	•2188- •0449-
300	97	581	50.00	•00	31+15 41+53	50.25	•00	2.1967	-0546-	•2014- •2552-	.0054	•0596-	.0274-
300	97	582	50.00	.00	62.29	50.49	•00	2.1069	.0513-	.2764-	.0021	.0104	0354
300	97	583	50.00	•00	103.82	50.81	•00	2,0981	.0522-	•2974-	.0031	•0468	.0818
300	98	584	55.00	•00	15.57		•00	2.4400	-0438-	+0041	.0069-	•1675-	-2271-
300 300	98 98	585 586	55.00 55.00	•00 •00		55.17 55.26	•00	2.2608	.0492- .0528-	•0601- •2756-	.0011- .0012	•1156- •0417-	•1657- •0553-
300	98	587	55.00	.00	41.53	55.35	.00	2.2450	.0535-	.3414-	.0003	0213-	.0034-
300	98	588	55.00	.00	62.29	55.51	•00	2.2026	-0561-	•3691-	.0010	•0276	•0426
300	98	589	55.00	•00	103.82	55.84	•00	2.1806	•0578-	•3591-	.0007	89د0•	•0584
300	99	590	60.00	•00	15.83	60.14	•00	2.4533	•0592-	.0757-	.0070	•0676	•1074
300	99	591 592	60.00	•00	21.10 31.65	60.19		2.3772 · 2.2700	.0678- .0630-	•1337- •2948-	.0010	•0754 •0391	•1491 •1973
300	99	593	60.00	.00	42.20	60.35		2.2309	0599-	•3568~	.0004	•0262	.1312
300	99	594	60.00	•00	63.30	60.52		2.2230	.0630-	.4016-	.0012	•0479	د 078 و
	100	596	65.00	•00	15.83	65.14		2.3765	.0502-	-1628-		•1078	-1554
	100	597	65.00	•00	21.10	65.18		2.3432	.0548-	.2184-	.0007-	•1537	•2190
	100	598 599	65.00 65.00	•00	31.65 42.20	65.27		2.3247	.0567-	•3760→ •4376−	•0022- •0013-	•1514 •1676	•1809 •0840
	136	600	65.00	.00	63.30	65.52		2.2036	.0574-	•4084-	.0011-	•0831	.0992
300	100	601	65.00	•60	105.50	65.89		2.2868	.0597-	•4475-	•0001	•0433	•0611
	101	602	70.00	•00	16.13	70.14		2.4060	.0534-	-2470-	-0001-	•0486	•0508
	101	603	70.00 70.00	•00	21.50	76.19		2.3598	•0496-	•3059-		•0901	•1452
	101 101	604 605	70.00	•00	32.25 43.00	70.27		2.2347	•0431- •6434-	•3685- •4606-	.0010- .0614-	•1319 •0807	•1865 •0934
300	101	606	70.00	•00	64.50	70.52		2.1909	•0437-	.4883-	.0025-	•0633	.0461
300	101	607	70.00	∙ũ∪	107.50	70.87	•00	2.1928	•0436-	•5255-	•002U-	•0290	8000
	102	608	80.00	.00		80.15		2.3731	•0224-	•4896-	.0004-	.0043-	•0022-
	102 102		80.00 80.00	•60	21.62	80.20 80.49	•00	2.3681 2.3396	•0257-	•4895~	.0004		.0134-
	102		80.00	.00	32.43 43.24	80.29	.00	2.3005	•0242- •0230-	•5728- •6541-	.0016-	•0080-	.0000
300	102	612	80.00	• 60	64.86	80.54	.00	2.2148	•0219-	•6384-	.0010-	•C115	•0167
300	102	613	80.00		108.10	80.90	.00	2.2347	•U300-	•7279-	.0017-	•3750	•0300
	103	614	90.00		16.28	90.14		2.3063	.0103-	•7159-	.0005-	-0314	•6066
	103 103		90.00 90.00	•00 •00		90.19 90.27		2.3207 2.2621	.0110- .0147-	•7733- •8624-	.0002 .0002-	+0013 +0050-	.0051 .0007
300	103	617	90.00	• 60	43.40	90.37	.00	2.2972	.0208-	.8188-	.0010-	.0011-	•C126
	103 103		90.00 90.00	•00		90.53		2.1943	•0295- 1 •0398-	.8399- .8762-	.0009-	•0020 •0177	.014z .0351
1						1							
		1548 1549	.0∪ 5.0∪	• () () • () ()	100.00	.00 5.12	.00	.0132 .3591	.0373 .0288	.0020- .0752-	.0004 .0006	*0009	•0000 •0013-
			10.00	.00	100.00	10.17	.00	4729	.0203	0428-	.0004	•0000	•0017-
400	301	1563	70.00	.00	16.13	70.18	•00	3.0270	.0161-	•9491-	•0021	•0715	•0855
→ ∪∪ 1									.0399-				
400		1564 1565	70.00 70.00	•60	32.25 107.50	70.34 71.15	•00 •03	2.8212	.0599-	1.1251-	.0152 .0008	•0887- •0121	•0857- •0250

 $^{{}^{\}dagger}\text{Minus signs}$ are to the right of the numbers to which they apply.

TABLE III. - AERODYNAMIC COEFFICIENTS OF MODEL FOR THE COMPLETE INVESTIGATION - Continued

Config.	Run	Point	α ₁ , deg	ø, deg	q, lb/sq ft	α, deg	β, deg	c _N	C _A	C _m	c,	Cn	CY
400 400 400	302 302 302	1566 1567 1568	80.00 80.00 80.00	•00 •00 •00	16.22 32.43 108.10	80.19 80.36 81.16	.00 .00	3.0578 2.9579 2.8997	.085 .0339- .0493-	1.1832- 1.3333- 1.4425-	.0017 .0029 .0015	•0051 •0520- •0193	.0220- .1113- .0321
400 400 400	303 303 303	1575 1576 1577	70.00 70.00 70.00	5.00 5.00 5.00	16.13 32.25 107.50	70:11 70:27 71:09	4.70 4.71 4.73	3.0963 2.8587 2.9356	.0531- .0472- .0645-	•9812- 1•1525- 1•3062-	.0105- .0139- .0142-	•0911 •1291- •0290-	.0674 .2190- .0342
400 400 400	304 304 304	1578 1579 1586	80.00 80.00 80.00	5.00 5.00 5.00	16.22 32.43 108.10	80.15 80.32 81.15	4.92 4.93 4.94	3.0170 2.9272 2.9563	.0444- .0444- .0597-	1.1469- 1.2887- 1.4645-	.0124- .0120- .0151-	•0396- •0046- •0482	.0502- .0275- .0048
400 400 400	305 305 305	1581 1582 1583	70.00 70.00 70.00	10.00 10.00 10.00	16.13 32.25 107.50	69.90 70.05 70.86	9.40 9.41. 9.45	3.1206 2.7917 2.8830	•(416- •(466- •(625-	.9833- 1.1738- 1.2929-	.0511- .0298- .0268-	•0686 •1127- •0151-	•0500- •3207- •1512-
400 400 400	306 306 306	1584 1585 1586	80.00 80.00 80.00	10.00 10.00 10.00	16.22 32.43 108.10	80.04 80.20 81.00	9.85 9.85 9.88	2.9647 2.8943 2.8650	•(280- •0441- •6457-	1.1544- 1.2479- 1.4392-	•0266- •0261- •0259-	•0150- •0157 •0555	•2825- •1230- •0744-
400 400 400	307 307 307	1587 1588 1589	70.00 70.00 70.00	5.00- 5.00- 5.00-	16+13 32+25 107+50	70.11 70.27 71.07	4.70- 4.71- 4.73-	2.9993 2.8963 2.8800	•0584- •0547- •0633-	.9348- 1.1159- 1.2681-	.0168 .0138 .0151	•0924 •0477- •0183	•1723 •0243 •0800
400 400 400	308 308 308	1590 1591 1592	80.00 80.00 80.00	5.00- 5.00- 5.00-	16.22 32.43 108.10	80.15 80.32 81.13	4.92- 4.93- 4.94-	3.0571 2.9057 2.9138	•0333- •0754- •0753-	1.1966- 1.2440- 1.4517-	.0144 .0138 .0147	.0312- .1727- .0009	•0754 •0953- •0943
400 400 400	309 309 309	1593 1594 1595	70.00 70.00 70.00	10.00- 10.00- 10.00-	16.13 32.25 107.50	69.90 70.05 70.86	9•40- 9•41- 9•45-	3.0312 2.8145 2.8735	•0560- •0+44- •0528-	•9297- 1•0941- 1•2581-	•0294 •0272 •0291	•0187 •0340- •0177	•1309 •0762 •1537
400 400 400	310 310 310	1596 1597 1598	80.00 80.00 80.00	10.00- 10.60- 10.60-	16.22 32.43 108.10	80.04 80.18 80.99	9•85- 9•85- 9•88-	2.9856 2.7353 2.8495	•1106- •0+69- •0>44-	1.2162- 1.1312- 1.3946-	•0062- •0265 •0286	•0178 •1493- •0122-	•2181 •0185- •1468
400 400 400 400 400 400	311 311 311 311 311 311	1599 1600 1601 1602 1603 1604	.00 2.00 4.00 6.00 8.00 10.00	• • • • • • • • • • • • • • • • • • •	100.00 100.00 100.00 100.00 100.00	.00 2.04 4.09 6.15 8.21 10.26	.00 .00 .00 .00	.0101 .1395 .2766 .4288 .5841 .7294	.0373 .0348 .0311 .0265 .0228 .0194	.0021 .0219- .0498- .0878- .1339- .1858-	.0005 .0004 .0005 .0006 .0005	.0001 .0005 .0007 .0006 .0004	.0001 .0015 .0014 .0012
402 402 402 402 402 402	312 312 312 312 312 312	1605 1606 1607 1608 1609 1610	.00 2.00 4.00 6.00 8.00	.00 .00 .00 .00	100.00 100.00 100.00 100.00 100.00	.02- 2.03 4.07 6.12 8.18 10.23	.000	.0540-\ .0727 .2173 .3642 .5035	.0.06 .0379 .0331 .0283 .0235	.0904 .0659 .0334 .0030 .0312- .0821-	.0003 .0004 .0005 .0006 .0006	.0002 .0012 .0015 .0013 .0010	.0023- .0026- .0027- .0016- .0012-
404 404 404 404 404	313 313 313	1611 1612 1613 1614 1615 1616	.00 2.00 4.00 6.00 8.00 10.00	.00 .00 .00 .00	100.00 100.00 100.00 100.00 100.00	2.00 4.05 6.11 8.16 10.21		.1230- .0116 .1485 .3109 .4523 .5997	.0+90 .0+51 .0388 .0335 .0188 .0138	.1885 .1587 .1259 .0869 .0506 .0020	.0006- .0007- .0005- .0004- .0000	.0029+ .0019- .0012- .0006- .0005-	.0060 .0044 .0045 .0027 .0014

 $^{^{\}dagger}$ Minus signs are to the right of the numbers to which they apply.

TABLE III. - AERODYNAMIC COEFFICIENTS OF MODEL FOR THE COMPLETE INVESTIGATION - Concluded

19A0 19A0	<u> </u>		deg	deg	q, lb/sqft	α, deg	β, deg	CN	CA	C _m	C¹	Cn	CY
	336	1689	50.00	.00	15.57	50.17	.00	2.9799	.0280-	7885-	•0163	•0985-	•1158-
	336	1690	60.00	•00	15.83	60-17	•00	2.9027	.0456-	7889-	.0033	•0961	1514
19A0 19A0	336 336	1691 1692	70.00 80.00	•00	16.13 16.22	70.18 80.19	•00	3.0205 2.9885	.0513- .0360-	1.1934-	•0036 •0040	•1045 •0681	•1613 •1097
19A0	337	1693	50.00	5.00	15.57	50.05	3.84	2.8665	.0300-	-8049-		•1014-	-1810-
19A0 19A0	337	1694 1695	60.00 70.00	5.00 5.00	15.83	60.07 70.11	4.33	2.8926 3.0224	.0363- .0442-	•7436- •9905-	.0058-	•1509 •1125	•1398 •0760
1940	337	1696	80.00	5.00	16.22	80.15	4.92	2.9771	.0324-	1.1742-	.0069-	.0508	-0164-
19A0	338	1697	50.00	10.00	15.57	49.74	7.66	3.0102	.0200-	-863⊍-	.0085-		•179i-
19A0 19A0	338	1698	70.00	10.00 10.00	15.83 16.13	59.78 69.89	8 • 6 6 9 • 4 0	2.8357	•0351- •0445-	•6862- •9345-		•1431 •0770	•0119-
1940	338	1700	80.00	10.00	16.22	80.04	9.85	2.9761	.0251-	1.2104-	.0165-	.0710	1435-
19A0	339	1701	50.00 60.00	15.00	15.57	49.17	11.46	2.7266	•0004	.8013-	•0072-	•1295-	-2555-
19A0 19A0	339 339	1702 1703	70.00	15.00 15.00	15.83 16.13	59.28 69.51	12.97	2.7050	.0160- .0399-	.8282- .8725-	•0183- •0211-	•0480- •0969	•4410- •3272-
19A0	339	1704	80.00	15.00	16.22	79.84	14.77	2.8761	•0109-	1.2178-	•0153-	•0788	•3097-
1980 1980	340 340	1705 1706	50.00 60.00	15.00 15.00	15.57 15.83	49.18 59.29	11.46 12.97	2.7896 2.7514	.0154- .0242-	.7536- .8341-	-0083-	•1619- •1082-	-2855-
1980	340	1707	70.00	15.00	16.13	69.51	14.09	2.8422	0340-	.8701-	•0210- •0225-	•1082-	•5189~ •3148~
1980	343	1708	80.00	15.00	16.22	79.82	14.77	2.8133	.0074-	1.1331-	•0183-	•0495	•3650~
1980 1980	341 341	1709 1710	50.00 60.00	10.00	15.57 15.83	49.74 59.78	7.65 8.66	2.9356	.0281- .0351-	•7577- •6679-	.0078- .0114-	•1733- •1226	•3789- •0009-
1980	341	1711	70.00	10.00	16.13	69.90	9.40	2.9762	.0440-	•9199-	0114-	•0549	1343-
1980	341	1712	80.00	10.66	16.22	80.04	9.85	3.0198	•0315~	1.1860-	•0141-	•0115	-د214٠
	342	1713 1714	50.00 60.60	5.00 5.00	15.57 15.83	50.05 60.07	3.84 4.33	2.8001	.0277- .0458-	•7686~ •7089-	•0073 •0033-	•1021- •1442	•2800- •1372
1980	342	1715	76.0u	5.00	16.13	70.11	4.70	2.9758	.0443-	.9077-	•0066-	•0442	-62260
1	342	1716	85.0u	5.60	16+22	80.16	4.92	3.1086	.0413-	1.1856-	•0073-	•0078	•0782-
19BO 19BO	343 343	1717 1718	50.00 60.00	•00	15.57 15.83	50.17 60.17	•00	2.8745 2.9104	.0251- .0420-	•7430- •7816-	•0094 •0022	•1660- •0042-	•2271- •0218
1980	343	1719	70.00	•00	16.13	70.19	•00	3.1481	.0472-	1.0368-	•0014	•0533	.0727
1980	343	1720	80.00	۵۵۰	16.22	80.19	•00	3.0643	•0389-	1.1864-	•0003-	•0067-	د 460.
	344 344	1721 1722	50.00 60.00	•60 •60	15.57 15.83	50.17 60.17	•00	2.8977	.0337- .0484-	.8608- .8780-	•014i	•0458-	•0340
	344	1723	70.00	•60	16.13	70.18	•00	3.0834	.0484-	1.1387-	•0038 •00∠9	•0822 •0370	•1700 •1060
OAB	344	1724	80.60	•60	16.22	80.19	•00	2.9745	•0295-	1.2608-	•0010	•0022	.0834
	345 345	1725 1726	50.00 60.00	5∙00- 5•0u-	15.57 15.83	50.06 60.07	3 • 84- 4 • 33-	2.8763 2.9068	•0319- •0455-	•8657- •8708-	.0091- .0086	•0360 •0459	•1569 •2423
.8A0	345	1727	70.04	5.60-	16.13	70.11	4.70-	2.9926	•0455-	1.0759-	•0113	•0382	.2149
	345	1728	80.00	5.00-	16.22	80.15	4.92-	3.0755	•6239-	1.2059-	•00∠6	•0934-	•0792
	346 346	1729 1730	50.00 60.00	10.00+ 10.00+	15.57 15.83	49.73 59.79	7.66~ 8.66~	2.7860 2.8798	•0289- •0471-	.8259- .8866-	-0040- •01ع4	+0491 +0435	•2222 •3211
840	346	1731	70.06	10.00-	16+13	69.89	9 • 40-	2.9113	.0561-	1.0512-	-0201	•0245	•32.1
	346	1732	80.GL	10.00-	16.22	80.63	9.85-	2.9489	•0322-	1.1741-	•C199	•0787-	-1778
	347	1733 1734	50.00 60.00	15.00- 15.00-	15.57 15.83	49.17 59.29	11.46-	2.7568	•0236- •6360-	-8769- -9030-	.0032 .0186	.0928 .0458	•3663 •4675
840	347	1735	70.00	15.00-	16.13	69.51	14.09-	2.8258	.0407-	1.0689-	.0239	.0238-	4546
i	347	1736	80.00	15.00-	16.22	79.82	14.77-	2.8284	0046-	1.3798-	.0120	-1046-	د∠0د•
	348 348	1737 1738	50.00 60.00	15.00- 15.00-	15.57 15.83	49.17 59.29	11.46- 12.97-	2.7060 2.8172	•0227~ •0443-	•8634- •9090-	•0072	•1715	-5307
880	348	1739	70.00	15.60-	16.13	69.51	14.09-	2.7177	-0443-	•9849-	.0204 .0213	•1456 •0608	.6164 .
	348	1740	80.66	15.60-	16.22	79.82	14.77-	2.7187	•0096	1.3182-	•0125	•0654-	•3516
1	349	1741 1742	50.00	10.00-	15.57 15.83	49.72 59.78		2.6926 2.7596	•0275- •0479-	•7810- •8261-	.0011- .0156	•1055 •1321	•3299 •4603
880	349	1743	70.00	10.60-	16.13	69.89	9.40-	2.9524	•0500-	1.0283-	.0206	•0819	-4107
1	1	1744	80.00	10.00-	16.22			2.9802		1.1530-	•0156		•2256
			50.00 60.00	5.00- 5.00-	15.57 15.83		3.84- 4.33-	2.9091 2.8860	.0334- .0515-	.8035- .8528-	.0039- .0116	•0675 •1718	•£315 •3944
880	350	1747	70.00	5.00-	16.13	70.11	4.70-	2.9568	•U509-	1.0477~	.0115	•1067	•2881
	- 1	1748	80.00	5.60-	16.22		4.92-	2.9900		1.1583-	•0094	•0329-	•1526
	351 351	1749 1750	50.00	.UU .UO	15.57 15.83			2.9491 2.8998	•0331- •0469-	•7104- •8394-		•0301 •2103	•1175 •3364
880	351	1751	70.00	•00	16.13	70.18	•00	2.9295	•0495−	1.0068-	+0040	•1291	•1990
880	351	1752	80.00	•00	16.22	80.19	•00	2.9934	-01:0-	1.2209~	•0010	•0716	د ۱۷۱۵

 $^{^{\}dagger}$ Minus signs are to the right of the numbers to which they apply.

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